

APPLICATION OF NEURAL NETWORKS IN ROBOTIC
CONTROL AND DESIGN OF MECHANISMS

CENTRE FOR NEWFOUNDLAND STUDIES

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RAGHU BALASUBRAMANIAN



**APPLICATION OF NEURAL NETWORKS IN
ROBOTIC CONTROL
AND DESIGN OF MECHANISMS**

By

© RAGHU BALASUBRAMANIAN, B.E.

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Abstract

Neural network has been widely used in various fields of robotics. In this work, the neural network analysis using backpropagation algorithm is applied to the inverse velocity analysis of robotic manipulators near the singularity points accounting for the tracking error and feasibility of joint velocities. The inverse computations using the pseudo-inverse of the Jacobian matrix are compared with those obtained by the neural network analysis. The results illustrated using examples of two well known manipulators show the advantages of using the present work. A new learning algorithm called LP-neuro method is then developed to solve neural network problems. In this algorithm, the weights are obtained by a combination of Linear Programming having a sparse coefficient matrix and a single variable non-linear optimization method. The results are illustrated by solving three different problems, two of which are useful in the on-line control of robotic manipulators.

The designs of a function generator and a four-bar mechanism whose coupler curve passes through nine specified points, have been carried out using neural network methods. The design problem has been solved using non-linear techniques which yield a weight matrix in each of the cases. The accuracy of the methods is also discussed. Finally, gain parameters required for the trajectory control are evaluated using non-linear optimization method. Neural network is then trained to evaluate the gain parameters based on error history of different trajectories.

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List of Symbols

$\{ \}$	vector
$[]$	matrix
\ddot{a}_p	acceleration of the end effector in the radial direction
e	error in joint position
\dot{e}	error in joint velocity
$f(\cdot)$	activation function
f_x^i, f_y^i	forces acting on link i
l_1, l_2	link lengths
v_i, a_i	Cartesian velocity and acceleration of i th joint respectively
v_t	velocity of the end effector in the tangential direction
x_i, y_i	precision points
$\{\dot{x}\}$	Cartesian velocity vector
$\{I\}, \{D\}, \{O\}$	input, desired, and output vectors respectively
$[J]$	Jacobian matrix
$[J^+]$	pseudo-inverse of Jacobian matrix
$k_{p1}, k_{p2}, k_{v1}, k_{v2}$	gain parameters
$[K_p]$	proportional gain matrix
$[K_v]$	velocity gain matrix
L_0, L_1, L_2, L_3	link lengths of four-bar mechanism
$[W], [V]$	weight matrices

$[W_1]$	weight matrix for acceleration analysis
$[W_2]$	weight matrix for torque analysis
$[W_{ij}]$	weight matrix connecting i th and j th layers
X_i, Y_i	coordinates of the nine-point path problem
δ_i	error in the i th layer
η	learning factor
θ_i	displacement of i th joint
$\dot{\theta}_i, \ddot{\theta}_i$	angular velocity and acceleration of i th joint respectively
λ	damping factor
σ_i, u_i and v_i	components of singular value decomposed matrix
τ^i	torque acting on link i
Θ_i	displacement of i th joint
$\{\dot{\Theta}\}$	angular velocity vector
$\dot{\Theta}_{max}$	upper feasible limit of angular velocity
$\ddot{\Theta}$	joint acceleration

Chapter 1

Introduction and Literature Survey

1.1 Introduction

Artificial Intelligence (AI) is applied in diversified fields to achieve faster and better results. They are useful for achieving computationally fast and approximate solutions of certain decision problems that are based on information of diverse criteria. Expert systems, Artificial Neural Networks (ANN), Knowledge-based representations etc., are examples of different tools used in the application of AI. Robotics is a field that requires such techniques because robots are often employed to work in hazardous environments impossible for human interactions, and where the calculations are numerous and complicated. In the recent past, ANN have proved quite useful in robotics. Fig. 1.1 shows the various fields in robotics in which ANN is being widely used.

Singularity avoidance, synthesis of mechanisms, finer control of the trajectories of robotic manipulators are still the topics that require further research. A new technique which optimizes the efficiency and speed would be of great help because of on-line computational requirements in the robotics area.

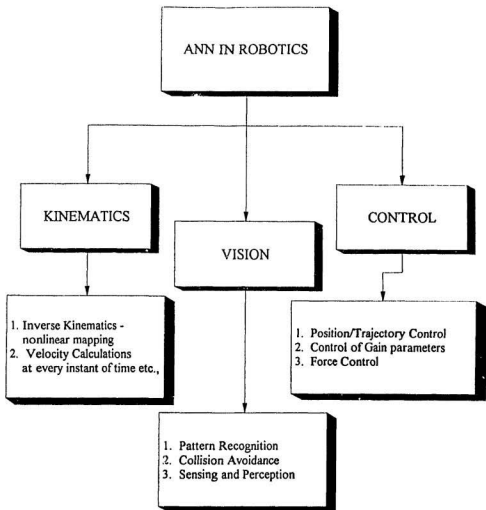


Figure 1.1 Application of Neural Network in Robotics

1.2 Literature Survey

1.2.1 Artificial Neural Network Methods

Artificial Neural Networks (ANN) have been studied for more than 30 years. Its use has increased tremendously in recent years because of the availability of faster and parallel processors and the basic learning algorithms (Grossberg, 1982; Hopfield, 1982; Rumelhart and McClelland, 1986; Kohonen, 1988). ANNs also referred as neural networks in this thesis are being used to accomplish complex functions such as generalization, error correction, information reconstruction, pattern analysis and learning. Neural network can learn mapping between the input and output space and synthesize an associative memory that retrieves the appropriate output when presented with an input, and has the ability to generalize with new inputs. Because of their massively parallel nature, neural networks can perform computations at very high speed (Fukuda and Shibata, 1992).

Neural networks have also been used to successfully solve complex problems like the Travelling salesman problem. It has been observed that neural networks have often been opportunistic, i.e. the network model is customized to serve the needs of the task at hand (Kulkarni, 1991). They represent a new approach that is robust and fault-tolerant.

Neural networks require basic algorithms for accomplishing the learning task. Several algorithms are functional in the present. One such algorithm which is widely used is backpropagation (BP) algorithm. In backpropagation algorithm, during the learning

phase, the observed outputs are compared with the desired outputs, and the weights are optimized to minimize the error function. In competitive learning, the weights are updated with each new input (Rumelhart and McClelland, 1986). Barmann and Biegler-Kong (1992) discuss efficient learning algorithms for neural networks.

Neural networks can perform functional approximations that are beyond the scope of optimal linear techniques. Gulati et al., (1990) have introduced neural formalism to efficiently learn non-linear mapping using a mathematical construct called terminal attractors.

Neural networks have been found useful in the field of robotics in the recent times. Forward and inverse displacement analyses of robotic manipulators have been done by Nyugen et al. (1990) and Gulati et al., (1990). Neural networks seem to be a promising approach to solve non-linear control problems as well (Tabary and Salaun, 1992). Some other interesting applications in the control of robotic manipulators can be seen in Fukuda et al., 1991; and Akio et al., 1992.

1.2.2 Singularity Problems in Robotics

Inverse kinematics problems of robotic manipulators are always difficult to solve because of (a) the multiple solutions in the displacement analysis problems, or (b) the occurrence of singularity points along the trajectories in the case of velocity analysis. The singularity problems, which involve the rank deficiency in the Jacobian Matrix, have been

dealt with by Chiaverni (1992). In this regard, general discussions on pseudo-inverse solutions can be seen in Lawson and Hanson, 1974. The pseudo-inverse solutions do not lead to satisfactory performance near the points of singularity because of abrupt changes in the elements of the joint velocity vector.

Damped-Least Squares method (DLS) approach has been used by many researchers (Wampler, 1986; Nakamura and Hanafusa, 1986; Maciejewski and Klein, 1989; Wampler and Leifer, 1988; Mayorga et al., 1992). The additional advantage with this method is that one can set the limit (achievable limit) on the norm of the joint velocity vector and find the corresponding damping factor, λ , which yields the minimum error. Maciejewski and Klein (1989) also proposed a truncated Singular Value Decomposition (SVD) solution method which could be used for on-line computations. However the resulting errors could be more in this method. So far, there has not been any method which takes into account factors such as the errors as well as the computational efficiency. Neural networks are known to perform well in those areas provided a relationship is established between the joint velocity vectors and Cartesian velocity vectors on an off-line basis. This circumvents the on-line computational requirements of the joint velocity vector, as was done by researchers mentioned earlier (Maciejewski and Klein, 1989).

1.2.3 Mechanism Synthesis

Synthesis of a mechanism is a means of finding the linkage that will produce the

specified motion. The problem of approximate synthesis of a four-bar mechanism whose coupler curve is a planar trajectory was solved by Wampler et al., (1992). Solution of such problems date as early as 1923 and some of the important works are given in Freudenstein and Sandor, 1959; Shigley and Uicker, 1980; Erdman and Sandor, 1984; Morgan and Wampler, 1989; Subbian and Flugrad, 1989. The use of optimization technique has been made by Suh and Radcliffe (1978). Angeles et al., (1988), or Akhras and Angeles (1990) have applied a variable-separation technique and non-linear optimization scheme to solve the four-bar path generation problem. Tsai and Liu (1989) have solved the nine-point path problem using a new continuation method. Wampler et al., (1992) have solved this problem using a combination of analytical and numerical tools. Problems where the number of points is greater than nine result in an over-determined system whose exact solutions are not possible.

The four-bar mechanisms have also been used in the design of function-generators. Freudenstein (1955) proposed an algebraic formulation for the approximate synthesis of such a mechanism. Wilde (1982) applied error linearization techniques to solve this problem. Other interesting references on such problems can be seen in (Mohan Rao et al., 1973; Tinubu and Gupta, 1984; and Liu and Angeles, 1992).

1.2.4 Neural Network Control in Robotics

There has been recent trend within the robotics control literature to apply neural networks for the control of robotic systems. In many applications reported in the

literature (Gu and Chan, 1989; Fukuda and Shibata, 1990; Helferty and Biswas, 1990; Jamshidi et al., 1990; Karakasoglu and Sundareshan, 1990; Yamamura et al., 1990) the process of neural network learning is conducted on-line (i.e. the dynamics of the neural network is embedded in the closed-loop with the dynamics of the robotic system), yet there appears to be a lack of studies focussing on the dynamic behavior of the neural network during learning and/or control when the neural network is used in such context.

Kawato (1990) used feedback error learning to compute the feedforward torques required for a manipulator to follow a path. The neural network implemented in this method uses the desired joint positions, velocities and accelerations as inputs and adjusts the network weights using the feedback torque as the error signal to a backpropagation parameter optimizing algorithm. Yuh (1992) also used a neural network for manipulator control. He used a "critic" equation, which is a function of the manipulator output error, to train the network to directly compute the manipulator input torques.

Asada (1990) used a multilayered feedforward network to learn a non-linear mapping for compliance control. From the measured forces and torques in an assembly task he used the network to compute the required velocities, which would allow the assembly task to be completed.

1.3 Thesis Objectives

We have seen in the last few sections that the neural networks are quite versatile

tools to solve problems in a wide variety of areas. With this in mind, it was thought to apply this tool to solve problems in the areas of mechanism design and robotic control. Based on this, the following are the objectives of this thesis:

- 1) Development of a new neural network learning algorithm (LP-neuro method) which is fast and accurate.
- 2) Application of neural networks for inverse kinematics of robotic manipulators near singular configurations and comparison with damped-least squares and pseudo-inverse methods.
- 3) Velocity, acceleration and torque analysis of robotic manipulators using neural networks.
- 4) Synthesis of mechanisms using neural networks
- 5) Trajectory control of the robotic manipulators using neural networks.

Chapter 2, briefly reviews the basics of neural networks. Backpropagation algorithm is introduced here and various factors influencing a neural network are discussed in this chapter. The significance of solving for weight matrix in neural network problems using combination of LP and a single variable non-linear optimization routine is identified here. The validity of the application of backpropagation algorithm is checked by using them near singular configurations of robotic manipulators. An inverse kinematic relationship is established between the Cartesian and joint velocities on off-line basis which reduces on-line computation time. The relative merits and demerits of this method over conventional pseudo-inverse and damped-least squares method are discussed in this

chapter. A new algorithm called LP-neuro method is developed to solve problems using neural networks.

In Chapter 3, the backpropagation method and the new algorithm called the LP-neuro method are then applied to solve various mechanism synthesis problems.

Chapter 4 deals with solution of non-linear or adaptive control problems. Here the non-linear control problem is solved using LP-neuro method developed in Chapter 2. Next, the gain values obtained by the non-linear method are then used in the neural control method where the methodology developed in sections 2.4.1 to 2.4.3 are used. In this way, the number of training sets required is a lot less than what many other researchers have used.

Finally, in Chapter 5, the contributions of the thesis and recommendations for future research are outlined.

Chapter 2

Neural Network Methods

2.1 Introduction

Neural network methods are widely used in many engineering applications. They can be thought of as a mathematical tool to solve common engineering problems such as optimization, pattern recognition etc. The *neural network* indicates the similarity of modelling network of neurons in the brain. Many linear and nonlinear neuron models are connected in the network and information is processed in a parallel distributed manner. This greatly reduces the computation time. Neural networks have learning and self-organization capabilities. They adapt to changes in data, learning the characteristics of the input signal.

Neural networks can be broadly classified into two types:

- 1) The neural networks that learn and adapt to changes are called recurrent networks or backpropagation networks. Multilayer perceptron neural nets, Hopfield nets, Adaptive Resonance Theory (ART) networks fall under this category.
- 2) Those that do not involve learning and sometimes called feedforward nets. Outer-product associative memories and multilayer nets without backward error

corrections belong to this type. The most popular neural networks used today are the Hopfield nets, Kohonen's self-organizing maps, multilayer perceptrons and ART nets.

Some of the operations that neural networks perform are shown in Fig. 2.1. They are advantageous in the following situations:

- 1) Decision-making from a massive amount of data
- 2) Non-linear mapping
- 3) Obtaining near-optimal solutions to optimization problem in less time.

2.2 Backpropagation Method

2.2.1 Multilayer Neural Network

A typical neural network is shown in Fig. 2.2. Basic components of a neural network are:

- 1) Input and output data sets
- 2) Weighed connections
- 3) Processing Elements (PE) or neurons
- 4) Activation function

The neural networks that need to be trained are supplied with predefined input and output data sets in a vector form. Each layer of a neural network consists of several processing elements. Each PE in a neural network sums all of its input values and performs a predefined operation and produces a single output value. PE's are connected with

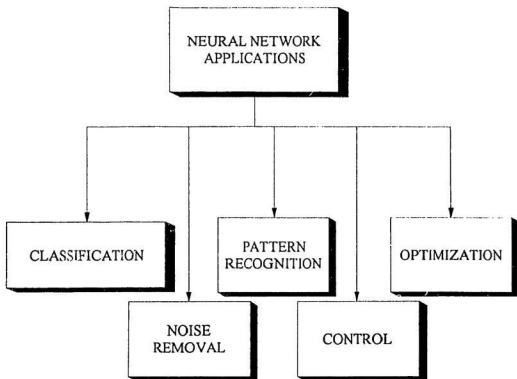


Figure 2.1 Applications of Neural Networks

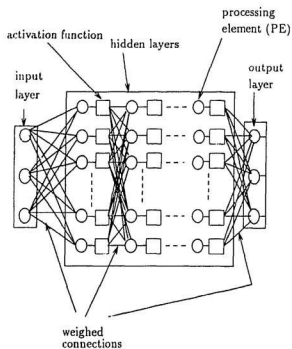


Figure 2.2 A Typical Neural Network

weighed connections. Information is stored in a network in the form of weights. In neural network method the weight matrix is obtained based on the learning process i.e., based on the input and output information used for that purpose.

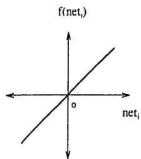
Activation functions, also known as squashing functions, perform mapping of PE's infinite domain into a prespecified range. Commonly used activation functions (shown in Fig. 2.3) are:

- 1) Linear activation function
- 2) Step activation function
- 3) Ramp activation function
- 4) Sigmoidal activation function or squashing function
- 5) Gaussian function

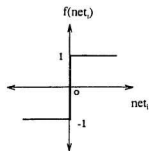
Neural networks are organized into several layers of PE's which include input layer, hidden layers and output layer as shown in Fig. 2.2. A feedforward network is one that has connections which feed information in one direction without any feedback path. If a network has feedback paths, then it is called feedback network. The training of multilayer neural networks depend on the following factors:

- 1) The number of layers
- 2) The number of PE in each layer
- 3) The amount of data needed for sufficient training.

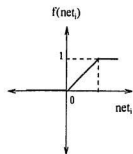
There are no predefined set of rules available for determining the above factors. Several techniques are available for the multilayer neural networks to have their connection



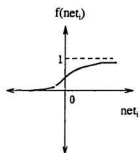
(a) Linear activation function



(b) Hard limiting function



(c) Threshold function



(d) Sigmoidal activation function

Figure 2.3 Activation Functions

weights adjusted to learn mapping. The most popular technique is the backpropagation algorithm (Werbos, 1974; Parker, 1982; Rumelhart, Hinton, and Williams 1986).

Learning process can be classified into two categories: supervised learning and unsupervised learning. Supervised learning monitors the duration of the training and the error performance etc., Unsupervised learning incorporates no monitoring process and relies only upon local information during the entire learning process. Most learning techniques are carried out off-line.

2.2.2 Feedforward Recall and Error Backpropagation Algorithm.

In neural network method, one establishes a relationship between the input and the desired output parameters. The matrix relationship between these two vectors are approximated by using several hidden layers as shown in Fig. 2.4. In this figure, the relationship between the input vector and the first hidden layer vector is at first expressed involving a weight matrix whose elements vary between -1 and 1 and are randomly generated. Similar procedure is adopted for the relationship between two adjacent hidden layers or the last hidden layer and the output layer. Mathematically, one of these typical relationships can be written as,

$$\{H\}_1 = [W]_1 \{I\} \quad (2.1)$$

where $\{I\}$ is the input vector and $\{H\}_1$ is the first hidden layer.

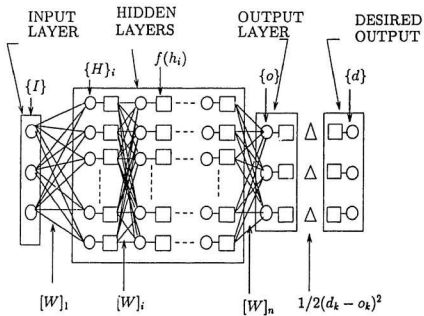


Figure 2.4 Representation of Neural Network Layers - Forward Computations

Next, values corresponding to sigmoidal function of each of the elements of the vector $\{H\}_1$ are computed and are symbolically represented by a square (\square) in Fig. 2.4. For example, for a typical element it would be written as

$$f(h_i) = \frac{1}{1 + \exp(-\alpha h_i)} \quad (2.2)$$

where α is the steepness factor and h_i is one of the elements of vector $\{H\}_1$. This process is continued until the last hidden layer i.e., each layer is related to other by a matrix containing weights, and also, there is a similar relationship written between the last hidden layer and the output layer.

Defining two vector $\{o\}$ and $\{d\}$ as the vector of output sigmoidal functions and desired values respectively, we wish to minimize the error E defined by

$$E = \frac{1}{2} \sum_{k=1}^N (d_k - o_k)^2 \quad (2.3)$$

Each of the summation terms (E_i) is represented by triangular (Δ) symbol in Fig. 2.4. This error has to be backpropagated using the same weights mentioned above. To do this, we first write the equation

$$\delta_{ok} = (d_k - o_k) (1 - o_k) o_k \quad (2.4)$$

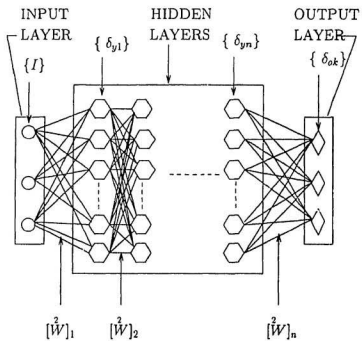


Figure 2.5 Representation of Neural Network Layers - Back-propagation of Errors

which is represented by a diamond symbol (\diamond) in Fig. 2.5. The error in the last hidden layer element wise is computed using

$$\delta_{yj} = y_j (1 - y_j) \sum_{k=1}^K \delta_{ok} w_{kj}, \quad j = 1, \dots, J \quad (2.5)$$

where y_j is the sigmoidal elemental output of the last hidden layer in Fig. 2.4 and w_{kj} is an element of the corresponding (to the right of y_j) weight matrix. This process is repeated until one computes all the elements of the first hidden layer. The weight matrix between the output layer and the last hidden layer to be used in the next cycle is recomputed as

$$[W_{kj}^2] = [W_{kj}^1] + \eta \{\delta_{ok}\} \{y_j\}^T \quad (2.6)$$

where the superscripts refer to the cycle number and η is the learning factor which is normally assumed between 10^{-3} to 10. The relationship for the weight matrix in other layers is given by

$$[W_{kj}^2] = [W_{kj}^1] + \eta \{\delta_{yj}\} \{y\}_{j-1}^T \quad (2.7)$$

Finally the weight matrix between the input and the first hidden layer is calculated using

$$[W_{kj}^2] = [W_{kj}^1] + \eta \{\delta_{yj}\} \{I\}^T \quad (2.8)$$

Once these weight matrices are obtained, then for any input vector one has to go through the forward computations as shown in Fig. 2.4 to obtain the output vector. This process is continued until the final set of weight matrices are obtained which yield the desired output values within the accuracy specified. Flowchart for the backpropagation method is shown in Fig.2.6.

2.2.3 Properties and its Significance

Backpropagation algorithm uses gradient descent technique to adjust the weights so as to minimize the error

$$\Delta w_k = -\eta \frac{\partial E}{\partial W_k} \quad (2.9)$$

where η is the step value. The movement of the weight vector in two-dimensional space can be observed on the error surface shown in Fig. 2.7. The weights of the network to be trained are typically initialized at small random values. The initialization strongly affects the ultimate solution. Another factor that affects the convergence is the steepness factor α , in the sigmoidal activation function given in Eq.(2.2). The effectiveness and convergence of the error backpropagation learning algorithm depend significantly on the value of the learning constant η . In general, however, the optimum value of η depends upon the problem being solved and there is no single learning constant suitable for different training cases. Activation functions with larger steepness factor produces the same effect as increasing the learning factor. So, the steepness factor is usually taken as

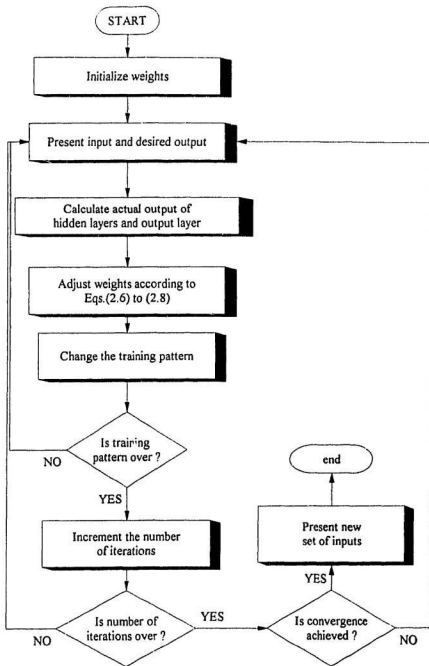


Figure 2.6 Flow Chart - Back-propagation Method

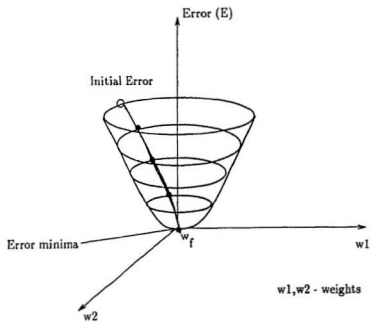


Figure 2.7 Movement of Weight Vector (2-D) on the Error Surface

1 and the learning factor is adjusted to control the convergence. However, gradient descent algorithm suffers from local minimum problem which is a common property of any nonlinear optimization algorithm.

2.2.4 Application - Singularity Problems in Velocity Analysis of Robots

When a manipulator is in singular configuration, it loses one or more degrees of freedom in the Cartesian space. Singularities in robotic manipulators may arise due to the geometrical limitations (constraints in the connecting links) of the manipulators. This problem can be handled by the use of redundant manipulators. There are two kinds of singularities:

- 1) Boundary singularities arise due to the geometrical limitations.
- 2) Interior singularities are due to two or more joint axes lining up.

Redundant manipulators also have singular configurations which have to be either avoided or handled. Near singular points, very high joint velocities result if the Cartesian velocities have components in the direction in which the arm loses mobility. These are the points at which the Jacobian matrix becomes rank-deficient.

While this problem can be handled using mathematical techniques like pseudo-inverse methods, yet it has certain limitations. The problems of singularities can be tackled at the task planning level itself by carefully designing the trajectory which avoids singular configuration. On the other hand, if due to wrong task planning or in situations

where on-line computations are made and the singularity appears in the trajectory, the robot control system must be able to pass through them safely. Multiple solutions exist at singularity points.

2.2.4.1 Velocity Analysis Using Psuedo-Inverse Method

The inverse kinematics for robotic manipulators is given by (Craig, 1986)

$$\{\dot{x}\} = [J] \{\dot{\theta}\} \quad (2.10)$$

where $\{\dot{\theta}\}$ represents the joint velocity vector and $\{\dot{x}\}$ is the end-effector velocity vector and $[J]$ is the Jacobian matrix. Therefore, the joint velocity corresponding to a given $\{\dot{x}\}$ is given by

$$\{\dot{\theta}\} = [J]^{-1} \{\dot{x}\}$$

$$\{\dot{\theta}\} = [J'] \{\dot{x}\} \quad (2.12)$$

where $[J']$ is called the pseudo-inverse of the Jacobian matrix. The basic idea is to minimize the norm $\|\{\dot{x}\} - [J]\{\dot{\theta}\}\|$ since $[J]^{-1}$ does not exist at singular points. $[J']$ gives an approximate solution satisfying the condition

$$\begin{aligned} \min \|\{\dot{\theta}\}\| \quad \text{and} \\ \min \|\{\dot{x}\} - [J]\{\dot{\theta}\}\| \end{aligned} \quad (2.13)$$

Near the singular points, $[J']$ is equivalent to $[J]^{-1}$ and pseudo-inverse finds out the exact solution. Though pseudo-inverse gives exact solution near singular points, they are not feasible because of very high values of $\{\dot{\theta}\}$. Hence a compromise is required between feasibility and exactness in case of inverse kinematic solution near singular points. Otherwise, pseudo-inverse solutions result in undesirable continuity leading to high joint velocity which results in very high oscillations.

2.2.4.2 Velocity Analysis Using the Damped Least Squares Method

Damped Least Squares (DLS) method has been proposed by several researchers to solve inverse kinematics problems. In this method, one writes the relation between $\{\dot{\theta}\}$ and $\{\dot{x}\}$ as

$$\{\dot{\theta}\} = [J]^T [J] + \lambda^2 [I]^{-1} [J]^T \{\dot{x}\} \quad (2.14)$$

In order to realistically achieve the desired joint velocity values, one must modify the above equation to suit the highest achievable limit of the manipulator in terms of angular velocities. In other words, we have to minimize the expression

$$\text{Min } \|\dot{x}\} - [J]\{\dot{\theta}\}\|^2 + \lambda^2 \|\{\dot{\theta}\}\|^2 \quad (2.15)$$

where λ is known as the damping factor. $\|\{\dot{\theta}\}\|$ is the norm of the joint velocity and the term $\|\{\dot{x}\} - [J]\{\dot{\theta}\}\|$ accounts for the minimization of the tracking error or exactness of the solution and $\lambda^2 \|\{\dot{\theta}\}\|^2$ takes care of the feasibility of the solution. It is equivalent to solving a minimization problem,

$$\begin{aligned} \text{Min } & \|\{\dot{x}\} - [J]\{\dot{\theta}\}\| \\ \text{subject to constraint} & \\ & \|\{\dot{\theta}\}\| \leq \dot{\theta}_{\max} \end{aligned} \quad (2.16)$$

where $\dot{\theta}_{\max}$ is practical limit on manipulators joint velocity. An appropriate value of damping factor, λ , will give the desired solution. Damping factor, λ , is computed using (Maciejewski and Klein (1989))

$$\|\{\dot{\theta}_{\max}\}\|^2 = \|\{\dot{\theta}\}^\lambda\|^2 = \sum_{i=1}^r \left[\frac{x_i' \sigma_i}{\sigma_i^2 + \lambda^2} \right]^2 \quad (2.17)$$

where $x_i' = \{u_i\}^T \{\dot{x}\}$ and r is the rank of the matrix and σ_i , $\{v_i\}$ and $\{u_i\}$ are obtained

from Singular Value Decomposition (SVD) of the Jacobian matrix [J]. To express Eq.(2.17) in a simple manner one can write

$$\{\dot{\Theta}_{\max}\} = \begin{Bmatrix} \dot{\Theta}_1^* \\ \dot{\Theta}_2^* \\ \vdots \\ \dot{\Theta}_n^* \end{Bmatrix} \quad (2.18)$$

where superscript * represents the maximum allowable value for that particular joint. At first, one evaluates

$$\|\{\dot{\Theta}_{\max}\}\|^2 = \dot{\Theta}_1^{*2} + \dot{\Theta}_2^{*2} + \dots + \dot{\Theta}_n^{*2} \quad (2.19)$$

and then using Eqs.(2.18) and (2.19) and using a nonlinear optimization technique, finds the value of λ which would minimize the function

$$\left[\frac{x_1'\sigma_1}{\sigma_1^2 + \lambda^2}\right]^2 + \left[\frac{x_2'\sigma_2}{\sigma_2^2 + \lambda^2}\right]^2 + \dots + \left[\frac{x_r'\sigma_r}{\sigma_r^2 + \lambda^2}\right]^2 - \|\{\dot{\Theta}_{\max}\}\|^2 \quad (2.20)$$

The optimal value of λ is then substituted in the following equation to get the damped joint velocity vector

$$\{\dot{\Theta}^{(\lambda)}\} = \sum_{i=1}^r \left(\frac{\sigma_i}{\sigma_i^2 + \lambda^2} \right) \{v_i\} \{u_i\}^T \{\dot{x}\} \quad (2.21)$$

Unfortunately, both these methods, i.e., the pseudo-inverse as well as the DLS are,

expensive in terms of computations, and not suitable for on-line tasks. It is important to select an appropriate value of damping factor, λ . A low value of λ minimizes the tracking error and gives rise to undesirable high joint velocities. A high value of λ accounts for the robustness but leads to low tracking accuracy (Chiaverini, 1992). The term $\sigma_i / (\sigma_i^2 + \lambda^2)$ far away from singular points, becomes (as $\lambda \rightarrow 0$)

$$\frac{\sigma_i}{\sigma_i^2 + \lambda^2} \approx \frac{1}{\sigma_i} \quad (2.22)$$

DLS solution overcomes two main limitations of pseudo-inverse solution near singular configurations namely the discontinuity and infeasible high joint velocities. But SVD calculations are computationally expensive and error compromise is high. In theory, it is possible to calculate the damping factor λ at each of the points along the trajectory (near singular points) but an optimal value of λ , if chosen for all the points would minimize the computational burden.

2.2.4.3 Velocity Analysis Using Neural Network Method

A single layer neural network is capable enough to learn the relationship between the Cartesian and joint velocities near singular configurations. This is a highly non-linear mapping where joint velocities increase at a higher rate.

Considering the fact that in the real-time control problems one has to keep in mind

both, the errors (displacement, velocity, force etc.), as well as the computational efficiency (real-time computations): therefore, in the present work, the relationship between the Cartesian velocity and the joint velocity vectors was established on off-line basis using the neural networks over a segment of a trajectory. This circumvents the on-line computational requirements of the joint velocity vector, as was done by researchers (Maciejewski and Klein, 1989) mentioned earlier in Chapter 1. In their method, the calculations were required to be done on a point by point basis but which results in the slowing down of the actual task. The additional benefit of the neural network method is that one can achieve better accuracy also.

The input vector is the Cartesian velocity vector and the output vector is the joint velocity vector. The training is performed on either side of the singularity point (Sharan and Balasubramanian, 1993). The following points are kept in mind while performing the training:

- 1) Maintain the joint velocities close to the upper feasible limit near the singular point.
- 2) A smooth transition curve of joint velocities is required on either side of singularity points.
- 3) Minimize the errors between the actual and achievable joint velocities.
- 4) Have optimal number of training tasks to achieve the non-linear mapping.

2.2.4.4 Case Study

To illustrate the theory developed so far, the task of moving the end effector along a trajectory consisting of a segment of a circle and a radial line is shown in Fig. 2.8. The point of singularity was the point B in this figure. While performing the task a constant tangential velocity along the radial path was desired. This task was performed using (a) A planar two degrees of freedom (DOF) manipulator (b) PUMA-560 manipulator. These are typical manipulators widely used by various researchers in the field of robotics.

A Planar Two-Link Manipulator

A simple two-link manipulator is shown in Fig. 2.9. The velocity relationships between joint velocity and the Cartesian velocity for this manipulator is given by

$$\begin{pmatrix} \dot{x} \\ \dot{y} \end{pmatrix} = \begin{bmatrix} J_{11} & J_{12} \\ J_{21} & J_{22} \end{bmatrix} \begin{pmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \end{pmatrix} \quad (2.23)$$

where x and y are coordinates of the path followed by the end-effector expressed in universal frame. The inverse of the Jacobian is written as

$$[J]^{-1} = \frac{1}{l_1 l_2 s_2} \begin{bmatrix} l_2 c_{12} & l_2 s_{12} \\ -l_1 c_1 - l_2 c_{12} & -l_1 s_1 - l_2 s_{12} \end{bmatrix} \quad (2.24)$$

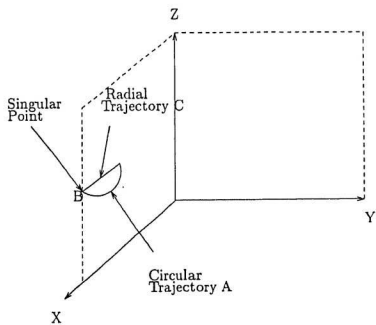


Figure 2.8 Trajectory Used for PUMA-560 Manipulator

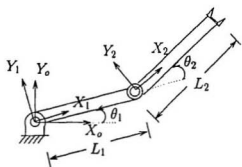


Figure 2.9 A Planar Two-Link Manipulator

where $c_1 = \cos\theta_1$; $s_1 = \sin\theta_1$; $s_2 = \sin\theta_2$; $s_{12} = \sin(\theta_1 + \theta_2)$; and $c_{12} = \cos(\theta_1 + \theta_2)$. Here, θ_1 and θ_2 are the joint angles of the manipulator and l_1 and l_2 are the link lengths. One can find from the above equation, the singularity arises when $s_2 = 0$ ($\theta_2 = 0$) i.e. when as the arm stretches outward and both joint rates go to infinity. The two-link manipulator is moving its tip at a constant tangential velocity of 0.03 m/s. The link lengths used were $l_1 = 0.4$ m and $l_2 = 0.2$ m; the radius of the circle was 0.07 m and the damping factor λ obtained from nonlinear optimization routine was 0.0077.

PUMA-560 Manipulator

The forward kinematic relationship between Cartesian coordinates and joint coordinates for a PUMA-560 manipulator (shown in Fig. 2.10) is given by

$$\begin{aligned} x_o &= a_3 c_1 c_{23} - d_4 c_1 s_{23} + a_2 c_1 c_2 - d_3 s_1 \\ y_o &= a_3 s_1 c_{23} - d_4 s_1 s_{23} + a_2 s_1 c_2 - d_3 c_1 \\ z_o &= -a_3 s_{23} - d_4 c_{23} - a_2 s_2 \end{aligned} \quad (2.25)$$

The link parameters for this manipulator are shown in Table 2.1. While performing the task, the desired tangential velocity along the circular path for PUMA-560 was 0.5 m/s and it was the same velocity along the radial path also. The maximum achievable limit $\dot{\Theta}_{\max}$ for each of the manipulators was taken to be 25 rad/s.

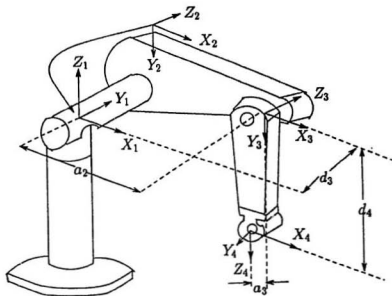


Figure 2.10 PUMA-560 Manipulator

Table 2.1 Link Parameters of PUMA-560 Manipulator

Link i	α_i	θ_i	H_i	D_i
	(degrees)	(degrees)	(m)	(m)
1	0	θ_1	0	0
2	-90	θ_2	0.4318	0
3	0	θ_3	0.02032	0.127
4	-90	θ_4	0	0.4318

2.2.4.5 Results and Discussion

At first a PUMA-560 manipulator is considered. The $\{\dot{\theta}\}$ vector was obtained using Eqs. (2.11) or (2.12) depending upon the proximity of the point to the point of singularity. The results obtained are shown in Figs.2.11 to 2.14. Similarly, the results for damped least squares method using Eq.(2.21) are also shown in these figures. It is quite clear here that the required values near the point of singularity are high and not achievable because this manipulator has a maximum $\|\dot{\theta}\|$ equal to 25 rad/s. For the neural network analysis, the input and the output values for the learning phase were specified in accordance with Eqs. (2.11) or the maximum limits over the trajectory. After this, the weight matrix $[W]$ which relates $\{\dot{x}\}$ and $\{\dot{\theta}\}$ as

$$\{\dot{x}\} = [W] \{\dot{\theta}\} \quad (2.26)$$

was obtained using Eqs. (2.1) to (2.8). The results are shown in Figs. 2.11 to 2.14. In all these figures, the results obtained by neural network analysis are far more accurate than those obtained by the DLS method i.e. the neural network method gives the norm values much closer to the values given by Eqs. (2.11) and (2.12) than the DLS method. Secondly, the error in $\|\dot{x}\|$ (to the right of point B) in Fig.2.14 in the case of neural network method, is due to the maximum achievable limit and not due to the method itself. In addition, as mentioned earlier, the DLS method requires much more on-line computations. These facts were further confirmed in the case of two-link manipulator as shown in Fig.2.9. The results in this case are shown in Figs. 2.15 to 2.18. The trajectory in this case was the same as used earlier.

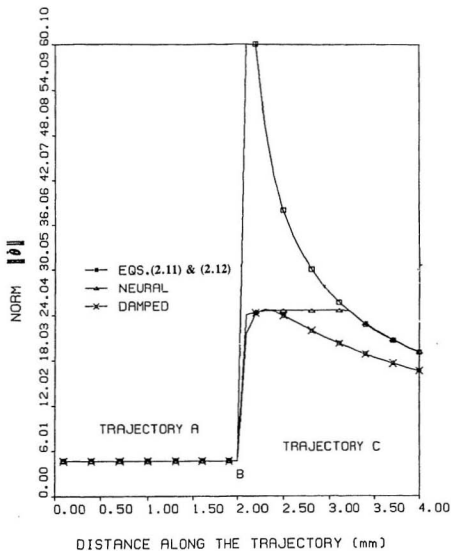


Figure 2.11 Variation of the Norm of the Angular Velocity Vector, $\|\dot{\theta}\|$, Along the Trajectory of a PUMA-560 Manipulator

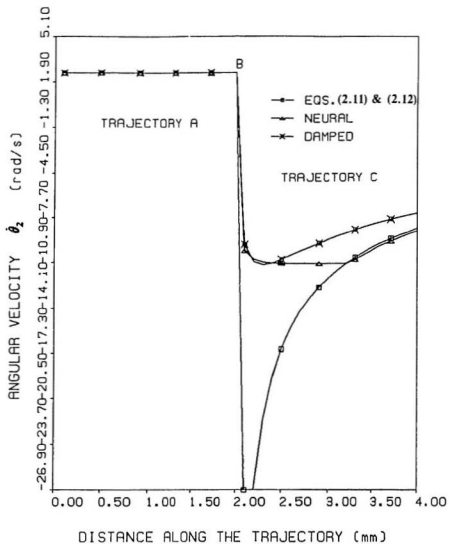


Figure 2.12 Variation of the Angular Velocity, $\dot{\theta}_2$, Along the Trajectory of a PUMA-560 Manipulator

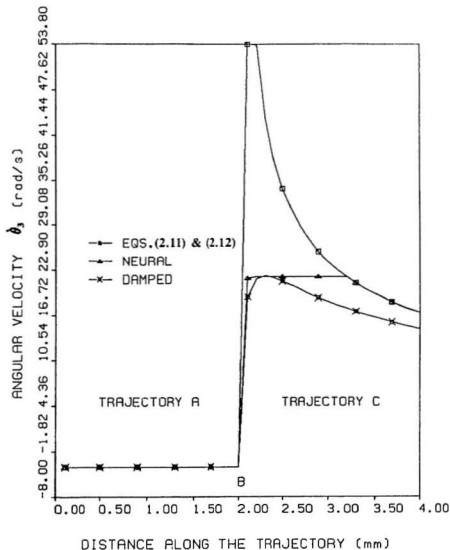


Figure 2.13 Variation of the Angular Velocity, $\dot{\theta}_3$, Along the Trajectory of a PUMA-560 Manipulator

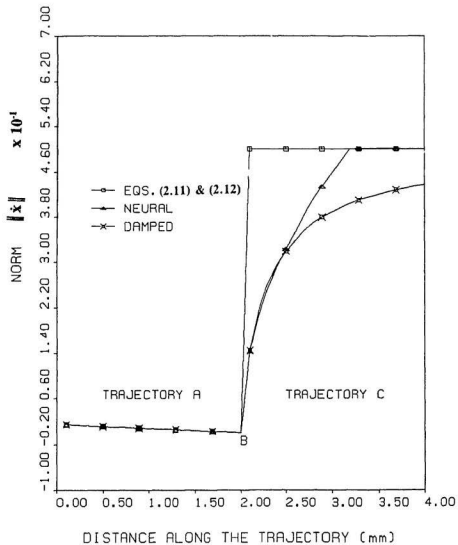


Figure 2.14 Variation of the Norm of the Cartesian Velocity Vector, $\|\dot{x}\|$, Along the Trajectory of a PUMA-560 Manipulator

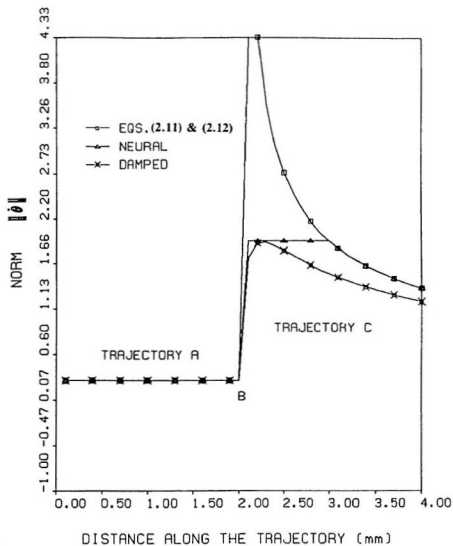


Figure 2.15 Variation of the Norm of the Angular Velocity Vector, $\|\dot{\theta}\|$, Along the Trajectory of a Two-Link Manipulator

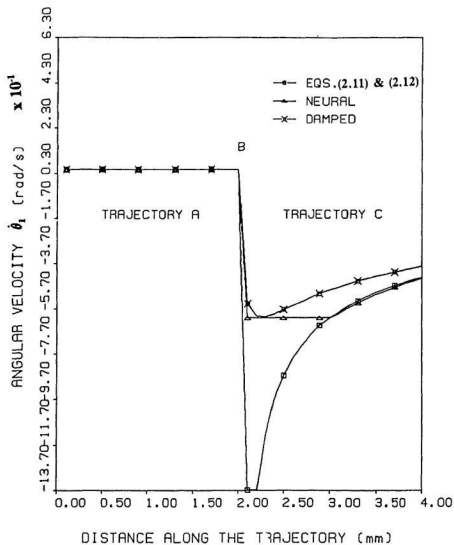


Figure 2.16 Variation of the Angular Velocity, $\dot{\theta}_1$, Along the Trajectory of a Two-Link Manipulator

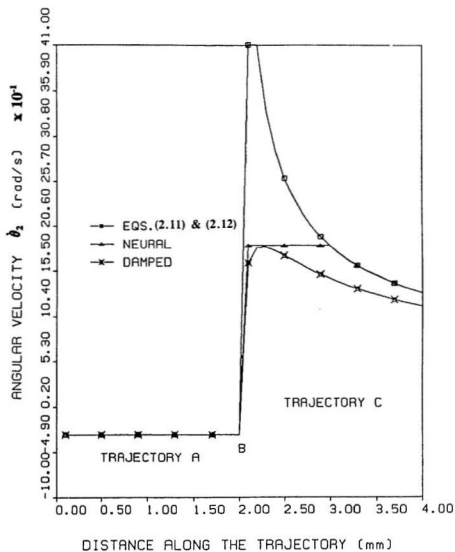


Figure 2.17 Variation of the Angular Velocity, $\dot{\theta}_2$, Along the Trajectory of a Two-Link Manipulator

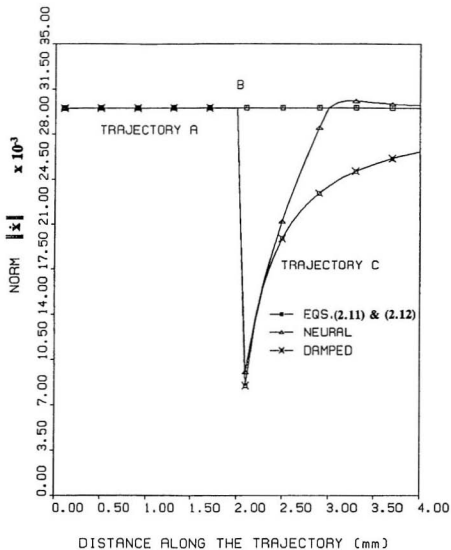


Figure 2.18 Variation of the Norm of the Cartesian Velocity, $\|\dot{x}\|$, Along the Trajectory of a Two-Link Manipulator

2.3 LP-Neuro Method

2.3.1 A New Approach - Development of LP-Neuro Method

As discussed earlier, a method to trade-off the accuracy and computational efficiency, is sought. A new method called LP-neuro method (Balasubramanian and Sharan, 1993) is developed in this section which utilizes the faster convergence property of linear programming; this result in better error minimization. The architecture of this method is similar to the feed forward error backpropagation neural network except that a single layer is enough. The activation function used in this case is a linear activation function with slope m and intercept c . A nonlinear curve is approximated by several linear curves of different slopes and intercepts. The error minimization objective function has weights and intercepts as linear variables and the slope as non-linear variables which is solved using Hooke and Jeeves method.

2.3.1.1 LP-Neuro Method - Type 1

In the neural network method (as used in Sec. 2.2.4.3), the input $\{I\}$ and desired output $\{D\}$ vectors are related by the equation

$$\{D\} = [W] \{I\} \quad (2.27)$$

However, due to errors, one obtains a vector $\{O\}$ instead of $\{D\}$. The weight matrix $[W]$ which relates the input and output vector in that case is given by

$$\{ H \} = \begin{Bmatrix} h_1 \\ h_2 \\ \vdots \\ h_j \end{Bmatrix} = \begin{bmatrix} w_{11} & w_{21} & \cdots & w_{k1} \\ w_{21} & w_{22} & \cdots & w_{k2} \\ & \vdots & \vdots & \\ w_{j1} & w_{j2} & \cdots & w_{jk} \end{bmatrix} \begin{Bmatrix} i_1 \\ i_2 \\ \vdots \\ i_k \end{Bmatrix} \quad (2.28)$$

The LP-neuro method is diagrammatically explained in Fig. 2.19. The functional relationship between $\{H\}$ and $\{O\}$ can be written as

$$o_j = f(h_j) = h_j \quad (2.29)$$

and

$$\{ O \} = [W]\{ I \} \quad (2.30)$$

The element o_j is shown by a square symbol (\square) in Fig. 2.19 and h_j are the elements of vector $\{H\}$. This is similar to the sigmoidal functional relationship used in backpropagation method, where one uses the equation

$$o_j = f(h_j) = \frac{1}{1 + \exp(-h_j)} \quad (2.31)$$

One of the ways to obtain the set of weight matrices with minimum error would be by

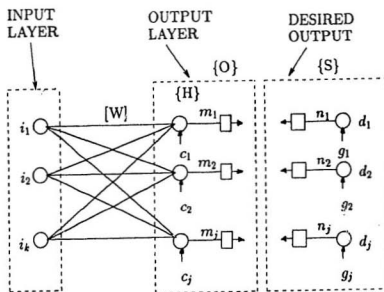


Figure 2.19 Diagrammatic Representation of the Network - LP-Neuro Method

writing a cost function E in the following form:

$$\text{Minimize } E = (d_1 - o_1) + (d_2 - o_2) + \dots + (d_j - o_j)$$

or

$$\text{Minimize } E = (d_1 + d_2 + \dots + d_j) - (w_{11}i_1 + \dots + w_{jk}i_k)$$

Subject to

$$\begin{aligned} w_{11}i_1 + w_{12}i_2 + \dots + w_{1k}i_k &= d_1 \\ &\vdots \\ w_{j1}i_1 + w_{j2}i_2 + \dots + w_{jk}i_k &= d_j \end{aligned} \quad (2.32)$$

where d_i are the elements of the desired output vector $\{D\}$ in Eq. (2.27), and w_{jk} are the weights. Eq. (2.32) has $(j \times k)$ weights and they can be collected in a single dimensional array or a vector as

$$\{W\} = \begin{Bmatrix} w_{11} \\ w_{12} \\ \vdots \\ w_{jk} \end{Bmatrix} = \begin{Bmatrix} w_1 \\ w_2 \\ \vdots \\ w_{j \times k} \end{Bmatrix} \quad (2.33)$$

This vector $\{W\}$ contains $j \times k$ unknowns. Since these can take positive or negative values, each of these can be replaced by two positive variables (a requirement for solving linear programming). For example, one can write $w_1 = v_1 - v_2$, $w_2 = v_3 - v_4$ etc. Substituting w_i in terms of v_i , one can rewrite the Eq. (2.32) as

$$\begin{aligned}
&\text{Minimize } E = (d_1 + d_2 + \dots + d_k) - (i_1 v_1 - i_1 v_2 + i_2 v_1 - i_2 v_3 + \dots + i_1 v_{2k-1} - \\
&i_1 v_{2k-2} + \dots + i_1 v_{2k-1} - i_1 v_{2k-2} + \dots + i_k v_{2k-1} - i_k v_{2k}) \\
&\text{Subject to} \\
&[A]\{V\} = \{D\}
\end{aligned} \tag{2.34}$$

The details of the coefficient matrix $[A]$ can be shown as

$$[A] = \begin{bmatrix} i_1 & -i_1 & i_2 & -i_2 & \dots & i_k & -i_k & 0 & 0 & 0 & 0 & 0 & 0 & \dots & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & i_1 & -i_1 & i_2 & -i_2 & \dots & i_k & -i_k & \dots & 0 & 0 & 0 & 0 & 0 & 0 \\ \vdots & \cdot & \cdot & \cdot & \cdot & \vdots & \cdot & \vdots & \cdot & \cdot & \cdot & \cdot & \vdots & \vdots & \cdot & \cdot & \cdot & \cdot & \vdots & \cdot & \cdot \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & \dots & i_1 & -i_1 & i_2 & -i_2 & \dots & i_k & -i_k \end{bmatrix} \tag{2.35}$$

Just like $\{W\}$, one can also write

$$\{V\} = \begin{Bmatrix} v_1 \\ v_2 \\ \vdots \\ v_{2k} \\ \vdots \\ v_{2jk} \end{Bmatrix} \tag{2.36}$$

The matrix [A] contains a number of zeroes in a given row. Here the non-zero elements occur together and only once in a given row. It is well known that the optimal cost function for such problems, involving sparsity, can be obtained much more quickly (McCormick, 1990) as compared to a case where [A] is a dense matrix.

2.3.1.2 LP-Neuro Method - Type 2:

Further refinements on the above method can be made by replacing the activation function given in Eq. (2.29) by another function given by

$$f(h_j) = m_j h_j + c_j \quad (2.37)$$

In Eq.(2.37) each variable h_j has a corresponding scalar m_j and a constant c_j . The new relationship corresponding to Eq. (2.30) will be

$$\{O\} = [M] \{W\} \{I\} + \{C\} \quad (2.38)$$

where [M] = diagonal slope matrix, which has scalar m_j as its diagonal elements.

A similar activation function for the output side can be written as

$$\{S\} = [N] \{D\} + \{G\} \quad (2.39)$$

where [N] is a diagonal matrix. The matrices [N] and {G} are analogous to [M] and {C} in Eq. (2.38). The new formulation using Eqs. (2.38) and (2.39) will be

$$\text{Minimize } E_i = [N]\{D\} + \{G\} - [M][W]\{I\} - \{C\}$$

subject to

$$[M][W]\{I\} + \{C\} = [N]\{D\} + \{G\}$$

or in the scalar form, it can be rewritten as

$$\begin{aligned} \text{Minimize } E_i = & n_1 d_1 + n_2 d_2 + \dots + n_j d_j - m_1 \{w_{11} i_1 + w_{12} i_2 + \dots + w_{1k} i_k\} - m_2 \{ \\ & w_{21} i_1 + w_{22} i_2 + \dots + w_{2k} i_k\} - \dots - m_j \{w_{j1} i_1 + w_{j2} i_2 + \dots + w_{jk} i_k\} + g_1 + \\ & g_2 + \dots + g_j - c_1 - c_2 - \dots - c_j \end{aligned}$$

subject to

$$\begin{aligned} m_1 \{w_{11} i_1 + w_{12} i_2 + \dots + w_{1k} i_k\} + c_1 &= n_1 d_1 + g_1 \\ &: \quad : \quad : \\ m_j \{w_{j1} i_1 + w_{j2} i_2 + \dots + w_{jk} i_k\} + c_j &= n_j d_j + g_j \end{aligned} \quad (2.40)$$

Again here, the weights w_{jk} , c_j and g_j are replaced by two positive numbers as before in the following manner:

$$\begin{aligned} w_i &= v_i - v_{i+1} \\ c_i &= v_{ci} - v_{ci+1} \text{ and} \\ g_i &= v_{gi} - v_{gi} \quad i = 1, 2, \dots \\ & \quad i = 1, 3, \dots \end{aligned} \quad (2.41)$$

After these substitutions, one arrives at

$$\begin{aligned} \text{Minimize } E_i = & n_1 d_1 + n_2 d_2 + \dots + n_j d_j - m_1 (i_1 v_1 - i_1 v_2 + i_2 v_1 - i_2 v_3 + \dots) + m_2 (i_1 v_{2k+1} - \\ & i_1 v_{2k+2} + \dots) + m_3 (i_1 v_{3k+1} - i_1 v_{3k+2} + \dots) + m_j (\dots + i_k v_{2jk+1} - i_k v_{2jk}) + v_{g1} - v_{g2} + \dots \end{aligned}$$

(2.42) is non-linear because of the occurrence of product terms such as $m_j v_1 \dots$ etc. However, if this problem is combined with another multi-variable optimization problem containing all m_j only, then the problem involving the remaining variables can be solved by the linear programming method. Since, the number of variables far exceed the number of constraints, it would be better to solve for m_j using non-linear optimization and the remaining variables which include weights, by linear method. This method clearly differs from others because, for the majority of the variables (other than n_k), the linear method yields faster convergence as compared to totally non-linear method. The additional advantage in the linear method is that one can exploit the sparsity in $[A]$ matrix in Eq. (2.35). For example, if the iterative values of m_j are obtained from the non-linear method, and substituted in Eq. (2.42), then the resulting problem becomes linear and can be solved using the Revised Simplex Method (Siddal, 1982). The actual flow chart of the combined method is shown in Fig.2.20. In fact, one can attempt to solve using a single m value instead of j different m_j values and check for convergence. If results are satisfactory, then the problem can be reduced to single variable non-linear optimization problem followed by linear programming.

2.4 Applications of the LP-Neuro Method

2.4.1 Function Generation

Approximating a sine curve has been a test for non-linear mapping carried out by several researchers. The non-linear mapping of a sine curve using backpropagation is

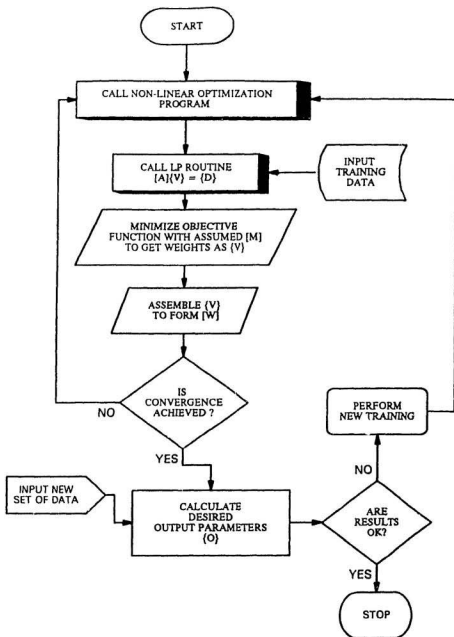


Figure 2.20 Flow Chart - LP-Neuro Method

described in (Zurada, 1992). The sine curve taken is

$$y = a \sin(bx) \quad (2.44)$$

where $a = 0.8$ and $b = \pi$. The same example was taken here for the case study. Instead of using several bias terms as done in Zurada (1992), a different approach was followed in the present work. To do this, 21 points along the sine curve in a period were taken for training. In order to identify this curve, the training was performed on different sine curves having different values of a and b . In all cases, 21 points were used. After this, the same number of points for this particular curve was provided as input and corresponding output was checked on the sine curve. The results using Eq. (2.34) and Eq. (2.44) are shown in Fig. 2.21. The results in this figure show that in the first quarter period, the BP method yields slightly better results than the LP method (Eq. 2.33) but not all through. On the other hand, the LP-neuro method (Eq. 2.41) is always accurate and decidedly the method to be used. In view of the above, only the LP-neuro method and BP method were used in the next two examples. Furthermore, a single value of m yielded results which were sufficiently accurate. Hence, the same procedure is followed in solving the next two examples.

2.4.2 Acceleration Analysis of a Two-link Planar Manipulator

A two-link planar manipulator having revolute joints is shown in Fig. 2.22. The end-effector, P, is made to follow a circular trajectory at a constant tangential velocity, v_1 , of magnitude equal to 0.15 m/s. (X_o, Y_o) represents the global coordinate system and

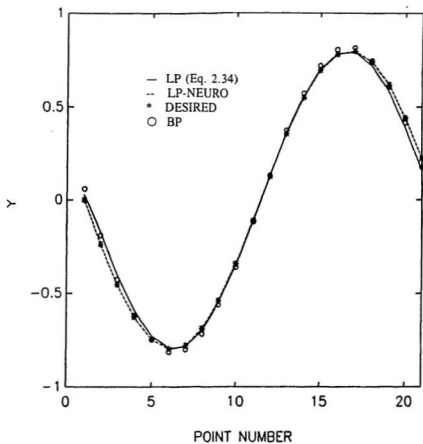


Figure 2.21 Comparison of Values for the Sine Curve (LP, LP-Neuro Method and BP Method and the Desired Values)

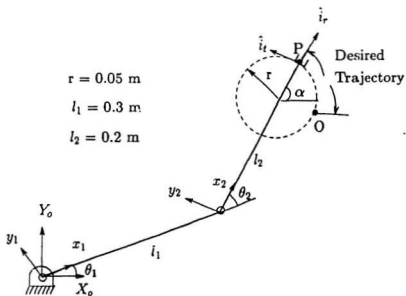


Figure 2.22 A Planar Two-Link Manipulator and the Trajectory used for Acceleration Analysis

(x_i, y_i) represent the local coordinate frame of the link i and the joint variables, θ_1 and θ_2 represent the rotational displacements.

The joint variables, θ_1 and θ_2 are related to the position of the end effector (X_p, Y_p) in Cartesian space through the following equations:

$$\theta_1 = \text{Atan2}(r_j, r_i) + \text{Atan2}(\sqrt{t}, r_k) \quad (2.45)$$

where $r_i = 2 Y_p l_1$; $r_j = 2 X_p l_1$; $r_k = Y_p^2 + X_p^2 + l_1^2 - l_2^2$; $t = r_j^2 + r_i^2 - r_k^2$;

and

$$\theta_2 = \text{Atan2}(Y_p - l_1 \sin \theta_1, X_p - l_1 \cos \theta_1) - \theta_1 \quad (2.46)$$

Differentiating Eqs. (2.45) and (2.46) with respect to time, we get

$$\begin{Bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \end{Bmatrix} = \begin{bmatrix} -l_1 s_1 - l_2 s_{12} & -l_2 s_{12} \\ l_1 c_1 + l_2 c_{12} & l_2 c_{12} \end{bmatrix}^{-1} \begin{Bmatrix} \dot{X}_p \\ \dot{Y}_p \end{Bmatrix} \quad (2.47)$$

where l_1, l_2 are the lengths of links 1 and 2 respectively; $c_1 = \cos \theta_1$; and

$c_{12} = \cos(\theta_1 + \theta_2)$ etc. The acceleration of the tip moving along the circular path in the radial direction is given by

$$\bar{a}_p = -\omega^2 r \hat{i}_r = \frac{-V_t^2}{r} \hat{i}_r \quad (2.48)$$

Resolving the tip acceleration in global coordinate system we get

$$\begin{Bmatrix} \ddot{X}_p \\ \ddot{Y}_p \end{Bmatrix} = \begin{Bmatrix} \frac{-V_t^2}{r} \cos(\alpha) \\ \frac{-V_t^2}{r} \sin(\alpha) \end{Bmatrix} \quad (2.49)$$

Here, one can obtain by differentiating the Eq. (2.49)

$$\begin{Bmatrix} \ddot{X}_p \\ \ddot{Y}_p \end{Bmatrix} = \begin{bmatrix} -l_1 s_1 & -l_2 s_{12} & -l_2 s_{12} \\ l_1 c_1 & l_2 c_{12} & l_2 c_{12} \end{bmatrix} \begin{Bmatrix} \ddot{\theta}_1 \\ \ddot{\theta}_2 \end{Bmatrix} + \begin{bmatrix} -l_1 c_1 \dot{\theta}_1 - l_2 c_{12}(\dot{\theta}_1 + \dot{\theta}_2) & -l_2 c_{12}(\dot{\theta}_1 + \dot{\theta}_2) \\ -l_1 s_1 \dot{\theta}_1 - l_2 s_{12}(\dot{\theta}_1 + \dot{\theta}_2) & -l_2 s_{12}(\dot{\theta}_1 + \dot{\theta}_2) \end{bmatrix} \begin{Bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \end{Bmatrix} \quad (2.50)$$

In robotic control, there is a great need for minimization of on-line computations. Rather than performing numerous computations as shown by Eqs. (2.45) to (2.50), it is desirable to find a linear relationship between the vectors given by

$$\begin{Bmatrix} \ddot{\theta}_{11} \\ \ddot{\theta}_{21} \\ \ddot{\theta}_{12} \\ \ddot{\theta}_{22} \\ \vdots \\ \ddot{\theta}_{in} \\ \ddot{\theta}_{2n} \end{Bmatrix} = [W_1] \begin{Bmatrix} r \\ \ddot{X}_{pl} \\ \ddot{Y}_{pl} \\ \vdots \\ \ddot{X}_{pn} \\ \ddot{Y}_{pn} \end{Bmatrix} \quad (2.51)$$

on the off-line basis first. The first subscript, i, in $\ddot{\theta}_{ij}$ represents angular acceleration of a particular link, and the second one, j, the point along the trajectory. The acceleration elements \ddot{X}_{pi} , \ddot{Y}_{pi} etc., are computed using Eq. (2.49).

In control problems, one needs to know $\{\ddot{\theta}\}$, as the end effector traverses the trajectory. Usually, on-line computations are done on a point by point basis i.e., one has to carry out computations given by Eqs. (2.45) to (2.50) at every point. In Eq. (2.51) above, if we obtain the $[W_1]$ on an off-line basis then, one can compute $\{\ddot{\theta}\}$ on an on-line basis for any set of points along the trajectory, much more rapidly. For training, circles

of different radii were used and in all cases 20 points were selected on different concentric circles. Figs. (2.23) and (2.24) show the results obtained by Eqs. (2.45) to (2.50). The same problem was also done using the BP method and shown in these figures. These figures clearly show that one can very successfully use neural network concept in general, and LP-neuro method in particular, in arriving at a better control strategy for robotic manipulators. The constant velocity requirement of the end effector is present in many industrial applications such as welding, painting etc.,

2.4.3 Solution of Torque and Reaction Forces of the Two-link Manipulator

The iterative Newton-Euler dynamics algorithm (see Table 2.2) has been used very extensively by various researchers. The link parameters used in this case are shown in Table 2.3. Here too, the number of computations is quite large to be performed on an on-line basis. In this method, kinematic solutions are carried out on a link by link basis starting from the base (refer to Fig. 2.22). When all the kinematic computations are completed, then the dynamic computations start from the outer link to the inner link. The details can be seen in (Craig, 1986) and are not mentioned here. Even in this case it would be better to have the following relationship on an off-line basis:

Table 2.2 The Iterative Newton-Euler Dynamics Algorithm

FORWARD RECURSION

- Step 1: $\{\omega\}_i = [R]_i^T \{\omega\}_{i-1} + \{z\} \dot{\Theta}_i$
 Step 2: $\{\alpha\}_i = [R]_i^T \{\alpha\}_{i-1} + \{z\} \ddot{\Theta}_i + [R]_i^T \{\omega\}_i \times \{z\} \dot{\Theta}_i$
 Step 3: $\{a\}_i = [R]_i^T (\{\alpha\}_{i-1} + \{\alpha\}_{i-1} \times \{p\}_{i-1} + \{\omega\}_{i-1} \times \{p\}_{i-1})$
 $+ \{z\} \ddot{\Theta}_i + 2 \times [R]_i^T \{\omega\}_i \times \{z\} \dot{\Theta}_i$
 Step 4: $\{a\}_i = \{a\}_i + \{\alpha\}_i \times \{s\}_i + \{\omega\}_i \times \{\omega\}_i \times \{s\}_i$
 Step 5: $\{F\}_i = m_i \{a\}_i$
 Step 6: $\{N\}_i = [I]_i \{\alpha\}_i + \{\omega\}_i \times ([I]_i \{\omega\}_i)$

BACKWARD RECURSION

- Step 7: $\{f\}_i = \{F\}_i + [R]_{i+1} \{f\}_{i+1}$
 Step 8: $\{n\}_i = [R]_{i+1} \{n\}_{i+1} + \{N\}_i + \{s\}_i \times \{F\}_i + \{p\}_i \times ([R]_{i+1} \{f\}_{i+1})$
 Step 9: $\tau_i = \{z\} \{n\}_i^T = n_z$

Table 2.3 Link Parameters of the Two-Link Manipulator

DETAILS	LINK 1	LINK 2	UNITS
LINK LENGTH	0.25	0.16	m
LINK CENTER OF GRAVITY	0.20	0.14	m
MASS	9.50	5.00	kg

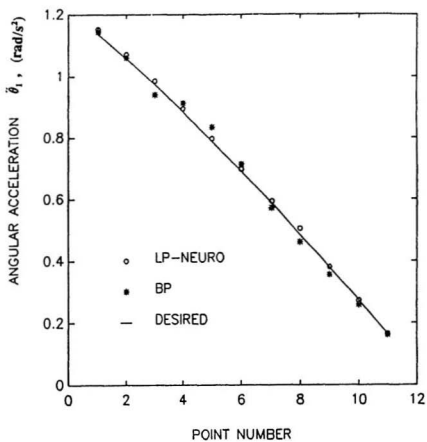


Figure 2.23 Variation of $\ddot{\theta}_1$, Along the Trajectory

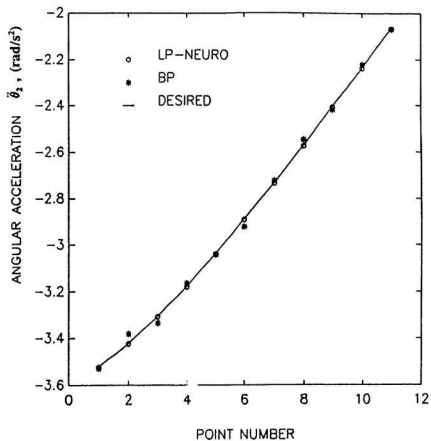


Figure 2.24 Variation of $\ddot{\theta}_2$, Along the Trajectory

$$\begin{Bmatrix} f_x^1 \\ f_y^1 \\ \tau^1 \\ f_x^2 \\ f_y^2 \\ \tau^2 \end{Bmatrix} = [W_2] \begin{Bmatrix} \theta_1 \\ \theta_2 \\ \dot{\theta}_1 \\ \dot{\theta}_2 \\ \ddot{\theta}_1 \\ \ddot{\theta}_2 \end{Bmatrix} \quad (2.52)$$

In Fig. 2.22, as the end effector P moves along the trajectory, due to the applied torques (τ^1 and τ^2) by the motors on the respective links, the reactions forces (f_x^1 , f_y^1 etc..) are produced. One has to know not only the torques but also these reactions forces at every point along the trajectory. The computations were carried out for the two-link manipulator along the shown trajectory. Twenty points were used here to obtain $[W_2]$. Results are shown in Figs. 2.25 to 2.30. The results clearly show that the overall error is quite small. It is less than 0.2 % in all the cases obtained by LP-neuro method. Such an accurate relationship would be of great help for on-line control of such systems. One can also see in these figures that LP-neuro method yields better results than BP method.

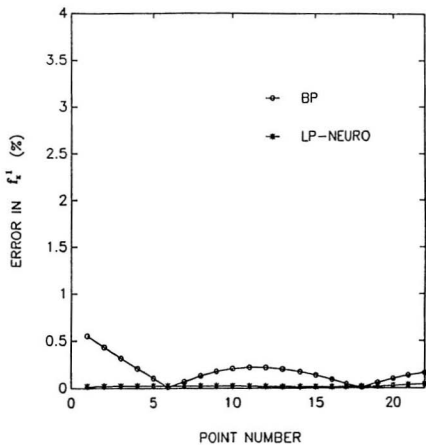


Figure 2.25 Error Values of f_x Acting on Link 1

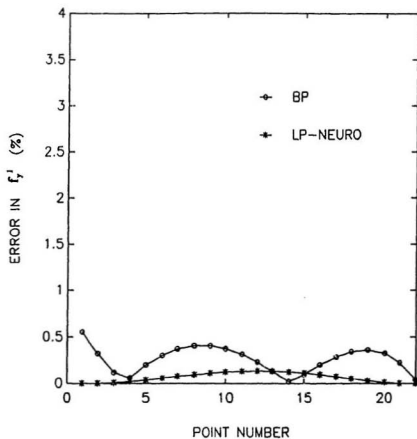


Figure 2.26 Error Values of f_y Acting on Link 1

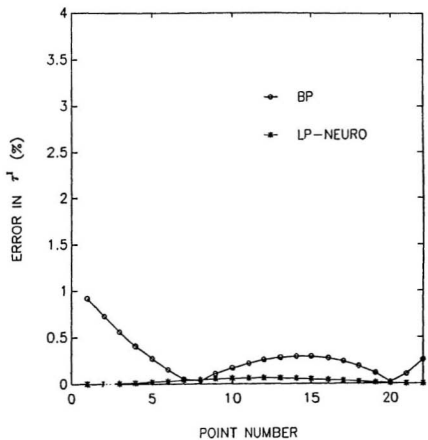


Figure 2.27 Error Values of τ_1 Acting on Link 1

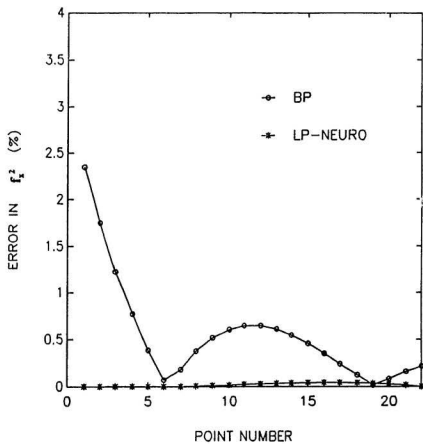


Figure 2.28 Error Values of f_x Acting on Link 2

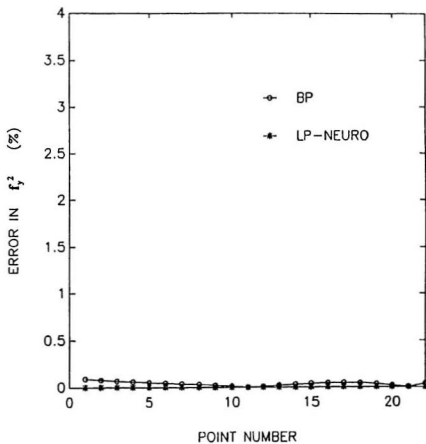


Figure 2.29 Error Values of f_y Acting on Link 2

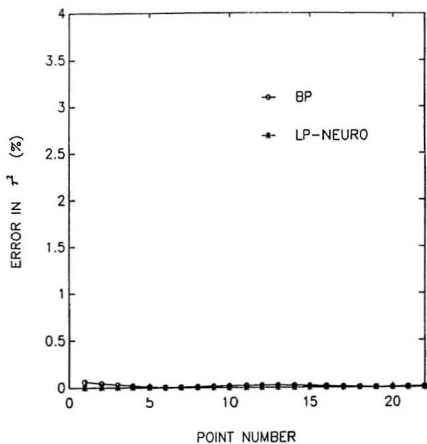


Figure 2.30 Error Values of τ_1 Acting on Link 2

2.5 Conclusions

In the velocity analysis near singular configurations, a mathematical relationship between the angular velocity and Cartesian velocity vectors was established using the DLS method and the neural network over a segment of a trajectory. The validity of this relationship was verified using two numerical examples.

Next in the LP-neuro method, the elements of the weight matrix were formulated as the unknown variables of the LP problem with equality constraints. These equations were then modified such that the coefficient matrix $[A]$ was sparse. In another case, a general linear relationship for the activation function was used and the resulting problem was solved using a combination of LP and a single variable non-linear optimization method. The utility of the algorithm developed was illustrated using three case studies, two of which had applications in the on-line control of robotic manipulators.

Based on the work in this chapter, the following conclusions can be drawn:

1. The neural network method yields more accurate results than the DLS method.
2. The neural network method established relationship over a segment of a trajectory rather than a point as in the case of the DLS method.
3. The neural network method is more suitable for on-line computations due to fewer computations required.
4. The results in all cases of the LP-neuro method showed that this method

yielded more accurate results than the BP method.

5. The use of LP-neuro method results in faster convergence as compared to BP method in all cases.

Chapter 3

Neural Networks in Mechanism Design

3.1 Introduction

In the last chapter, neural network methods were used to solve velocity analysis problems of robotic manipulators near the points of singularities and of the nonlinear acceleration relationships of such manipulators in the Cartesian space. Furthermore, neural networks were also used to establish the relationships for the torque calculations which could be used on on-line basis.

In this chapter, neural network techniques are used in the design of mechanisms namely the function generators as well as rigid body guidance mechanism involving coupler curves.

3.2 Implementation of Neural Network in Mechanism Design

3.3.1 Nine-Point Path Problem

A four-bar mechanism with an added coupler P is shown in Fig. 3.1. L_0, L_1, L_2, L_3 and L_4 are the link lengths and θ_1 and α are the angles shown in Fig. 3.1. The

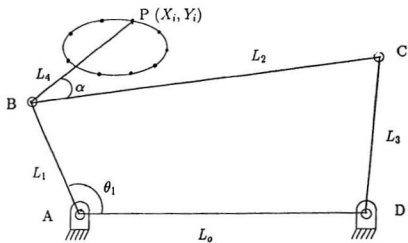


Figure 3.1 A Four-Bar Mechanism - Nine-Point Path Generation

objective is to find the necessary link parameters for the mechanism whose coupler point P passes through a given set of nine points. The constraint imposed here is that the link parameters should satisfy the Grashof's criterion i.e., the sum of the smallest and the longest link lengths cannot be greater than the sum of the remaining two link lengths if there is to be continuous relative rotation between two members.

The input consists of the co-ordinates of a set consisting of nine points and the output, the link parameters. The coupler point P goes through the nine points when θ_1 is varied in steps of 40° as shown in Fig. 3.1. The length of the fixed link l_{01} was chosen arbitrarily.

The mechanism is obtained using neural networks by first training it by providing the input data set

$$[I] = \begin{Bmatrix} Y_1 \\ Y_1 \\ X_2 \\ Y_2 \\ \vdots \\ X_9 \\ Y_9 \end{Bmatrix} \quad (3.1)$$

and the output

$$\{O\} = \begin{Bmatrix} L_1 \\ L_2 \\ L_3 \\ L_4 \\ \theta_1 \\ \alpha_1 \end{Bmatrix}^t \quad (3.2)$$

The superscript t refers to the first training set and the input and output relationship is governed by the displacement equation of the mechanism

$$\vec{R}_{PA} = \vec{R}_{BA} + \vec{R}_{PB} \quad (3.3)$$

By providing different number of data sets, one obtains the convergent weight matrix $[W]$.

The results obtained by both methods are shown in Tables 3.1 and 3.2. It is quite clear that the LP-neuro method yields better results but BP method also leads to good results.

**TABLE 3.1: LINK PARAMETERS OF FOUR-BAR MECHANISM -
NINE-POINT PATH GENERATION**

LINK PARAMETERS	LP-NEURO METHOD	BP METHOD
L_0	106.00 mm	106.00 mm
L_1	21.01 mm	20.54 mm
L_2	104.28 mm	105.62 mm
L_3	110.79 mm	111.95 mm
L_4	43.04 mm	42.01 mm
θ_1	53.49°	54.00°
α	15.58°	15.62°

**TABLE 3.2: COORDINATES OF THE NINE-POINT PATH PROBLEM -
COMPARISON BETWEEN THE LP-NEURO METHOD AND BP METHOD**

NO.	DESIRED		LP-NEURO METHOD		BP METHOD		LP- NEURO	BP
	X (mm)	Y (mm)	X (mm)	Y (mm)	X (mm)	Y (mm)	ERROR NORM	ERROR NORM
1	25.37	57.89	25.29	57.98	24.31	56.80	0.1204	1.5133
2	15.60	60.52	15.56	60.58	14.60	59.32	0.0721	1.5609
3	2.65	54.70	2.64	54.73	1.94	53.53	0.0316	1.3680
4	-6.70	43.00	-6.69	43.01	-7.09	41.98	0.0141	1.0927
5	-8.74	30.52	-8.73	30.53	-8.87	29.72	0.0141	0.8104
6	-3.45	22.79	-3.47	22.82	-3.47	22.20	0.0360	0.5903
7	6.51	23.69	6.44	23.72	6.44	23.19	0.0761	0.5048
8	17.70	33.59	17.59	33.64	17.38	32.98	0.1208	0.6888
9	25.88	47.53	25.77	47.61	25.12	46.65	0.1360	1.1627

3.3.2 Four-bar function generator

A typical four-bar function generator is shown in Fig. 3.2. The neural network method was used to design a four-bar function generator corresponding to

$$y = x^{1.5} \quad (3.4)$$

At first, the solutions were obtained for three precision points whose exact solutions were known (Wilson et al., 1983) and then for eight precision points. The precision points x_i were calculated by using Chebyshev spacing as follows:

$$x_i = x_o + \frac{\Delta x}{2} \left[1 - \cos(j\alpha - \frac{\alpha}{2}) \right] \quad j = 1, 2, \dots, n \quad (3.5)$$

where

$$\Delta x = x_f - x_o$$

n = number of precision points

α = $(180/n)$ degrees.

The linear relationship between θ and x is given by

$$\theta_j = \theta_o + \frac{\Delta \theta}{\Delta x}(x - x_o) \quad (3.6)$$

Similarly, we also have

$$\phi_j = \phi_o + \frac{\Delta \phi}{\Delta y}(y - y_o) \quad (3.7)$$

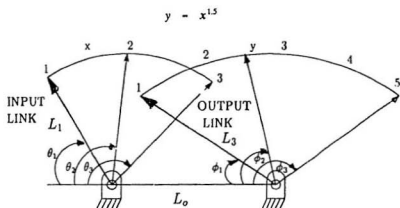


Figure 3.2 A Four-Bar Function Generator

The initial values x_o , θ_o , ϕ_o , as well as $\Delta\phi$, $\Delta\theta$, Δy and Δx are preselected. The objective was to find the necessary link parameters (L_o , L_1 , L_2 , L_3) which would yield accurate values at those precision points selected by using Eq.(3.5).

The network was trained using the input vector

$$\{I\} = \begin{Bmatrix} x_1 \\ y_1 \\ x_2 \\ y_2 \\ \vdots \\ x_n \\ y_n \end{Bmatrix} \quad (3.8)$$

and the output

$$\{O\} = \begin{Bmatrix} L_o \\ L_1 \\ L_2 \\ L_3 \\ \theta_1 \\ \vdots \\ \theta_n \end{Bmatrix} \quad (3.9)$$

The method consisted of the following steps:

1. Select three arbitrary values of x_i and a set of values for the link lengths.
2. Obtain θ_j corresponding to x_i using Eq.(3.6).

**TABLE 3.3: LINK LENGTHS FOR THE FUNCTION-GENERATOR MECHANISM -
THREE PRECISION POINTS**

LINKS	EXACT SOLUTION*	LP-NEURO METHOD
L_{q_0} (mm)	50.80	50.80
L_1 (mm)	264.16	263.83
L_2 (mm)	65.76	65.43
L_3 (mm)	255.52	255.78

* Refer Wilson et al. (1983)

**TABLE 3.4: COMPARISON OF y VALUES (THEORETICAL AND LP-NEURO
METHOD) - THREE PRECISION POINTS**

x	y_{th} (THEO.)	y_{lp} (LP-NEURO)	% ERROR (LP-NEURO) $= (y_m - y_{lp})/y_d * 100$
1.00	1.000	0.999	0.100
2.00	2.828	2.828	0.000
3.00	5.196	5.195	0.019

**TABLE 3.5: LINK LENGTHS FOR THE FUNCTION-GENERATOR MECHANISM -
EIGHT PRECISION POINTS**

LINKS	LP-NEURO METHOD
L_{a_0} (mm)	50.80
L_{a_1} (mm)	230.50
L_{a_2} (mm)	56.642
L_{a_3} (mm)	222.50

**TABLE 3.6: COMPARISON OF y VALUES (THEORETICAL AND LP-NEURO
METHOD) - EIGHT PRECISION POINTS**

NO.	x	y_{th} (THEO.)	y_{lp} (LP-NEURO)	% ERROR (LP-NEURO) $= (y_{th}-y_{lp})/y_{th} * 100$
1	1.019	1.029	1.029	0.000
2	1.169	1.264	1.261	0.237
3	1.445	1.737	1.715	1.266
4	1.805	2.425	2.368	2.350
5	2.195	3.252	3.170	2.521
6	2.555	4.084	4.011	1.811
7	2.831	4.763	4.719	0.923
8	2.981	5.144	5.122	0.427

3. Solve for ϕ_i corresponding to θ_i using displacement analysis of a four bar mechanism.

4. Obtain y_i using Eq.(3.7).

The results obtained for the link lengths of four-bar function generator for the three and eight precision points are given in Tables 3.3 to 3.6. Tables 3.4 and 3.6 show the errors in y values in function generators. It is quite clear from these tables, that the neural network can be successfully used to design function generators. Only the LP-neuro method was used here because it yielded better results than the BP method earlier.

3.4 Conclusions

The present work deals with the use of new techniques in the solution of design problems of different mechanisms. The set of weights which establishes the linear relationship were obtained using two non-linear methods. Based on the work in this chapter the following conclusions can be drawn:

1. The LP-neuro method yields better results than the BP method.
2. One can successfully use the neural network technique to solve the mechanism design problems.

Chapter 4

Neural Network Control in Robotics

4.1 Introduction

Much effort has been devoted to develop efficient procedures for real-time computation of manipulator dynamic equations. Recursive algorithms like Newton-Euler algorithm are now being used to achieve substantial improvement in terms of computational efficiency. In inverse dynamic calculations, the joint accelerations are affected not only by the computed torques but also by the disturbances such as Coulomb and viscous friction and modelling errors. The dynamic equations of a robotic manipulator form a complex, non-linear multivariable system. Computations are done at each point along the trajectory, which in turn reduce the overall speed of the movement of the manipulator.

In this chapter, an effort has been made to improve the computational need, by providing the gain parameters required to control the desired trajectory of a simple planar two-link manipulator using neural networks. Learning is based on input parameters like positional parameters $\{O\}$, error in position values $\{e\}$, error in joint velocity values $\{\dot{e}\}$ etc. A set of gain parameters namely position gain values k_p and velocity gain values k_v is identified using the LP-neuro method. Then the weights obtained are used in the on-

line trajectory control.

4.2 Trajectory Control

An independent Proportional-Plus-Derivative (PD) Control scheme is used to control the movement of the manipulator. While PD schemes are adequate in most control applications, there is overshooting i.e. the end-effector could go beyond the specified position before actually settling down. Overshooting is quite undesirable, because in order to eliminate overshooting, an integrator is used which introduces damping and causes the end-effector to move slowly through a number of intermediate set points, thus considerably delaying the completion of the task, and the quality of the displacement etc. The controller design can thus become more sophisticated on account of the involvement of non-linear system dynamics.

4.2.1 Inverse Dynamics of a n-Link Manipulator

The dynamic equation of an n-link manipulator in matrix form is written as

$$\{\tau\} = [M(\theta)] \{\ddot{\theta}\} + \{V(\theta, \dot{\theta})\} + \{G(\theta)\} \quad (4.1)$$

where

$[M(\theta)]$ is the mass matrix

$\{V(\theta, \dot{\theta})\}$ is the vector containing centrifugal and coriolis terms

$\{G(\theta)\}$ is the vector containing gravity terms

In the case of a simple planar two-link manipulator shown in Fig. 2.9, the matrices

involved are:

$$[M(\Theta)] = \begin{bmatrix} l_2^2 m_2 + 2l_1 l_2 m_2 c_2 + l_1^2 (m_1 + m_2) & l_1^2 m_2 + l_1 l_2 m_2 c_2 \\ l_2^2 m_2 + l_1 l_2 m_2 c_2 & l_2^2 m_2 \end{bmatrix} \quad (4.2)$$

$$\{V(\Theta, \dot{\Theta})\} = \begin{bmatrix} -m_2 l_1 l_2 s_2 \dot{\Theta}_2^2 - 2m_2 l_1 l_2 s_2 \dot{\Theta}_1 \dot{\Theta}_2 \\ m_2 l_1 l_2 s_2 \dot{\Theta}_1^2 \end{bmatrix}, \quad \text{and} \quad (4.3)$$

$$\{G(\Theta)\} = \begin{bmatrix} m_2 l_2 g c_{12} + (m_1 + m_2) l_1 g c_1 \\ m_2 l_2 g c_{12} \end{bmatrix} \quad (4.4)$$

These equations are derived using the Newton-Euler algorithm (shown in Table 2.2) based on the following assumptions:

1. All mass exists as a point mass at the distal end of the link.
2. Inertial tensor written at the center of mass for each link is the zero matrix.
3. There are no forces acting on the end-effector.

The idea of inverse dynamics is to seek a non-linear feedback control law

$$\tau = f(\Theta, \dot{\Theta}), \quad (4.5)$$

which when substituted in Eq.(4.1), results in a linear closed loop system. It is quite difficult or impossible to find control parameters for general non-linear systems. Since

$[M(\Theta)]$ is invertible, we may solve for joint acceleration $\{\ddot{\Theta}\}$ of the manipulator as

$$\{\ddot{\Theta}\} = [M]^{-1} \{ \{\tau\} - \{V(\Theta, \dot{\Theta})\} - \{G(\Theta)\} \} \quad (4.6)$$

To achieve control, a finite difference scheme where $\{\ddot{\Theta}\}$ and $\{\Theta\}$ are expressed in terms of $\{\tilde{\Theta}\}$ mentioned above, is used. This is discussed later in Section 4.3.1.

4.3 Evaluation of Gain Parameters for Trajectory Control

In a PD control scheme, the torque equation is given by

$$\{\tau_e\} = [K_p] \{e\} + [K_v] \{\dot{e}\} \quad (4.7)$$

where $\{e\} = \{\Theta_d(t+1)\} - \{\Theta_a(t)\}$ and

$$\{\dot{e}\} = \{\dot{\Theta}_d(t+1)\} - \{\dot{\Theta}_a(t)\}$$

From Fig. 4.1, the following observations can be drawn:

1. The kinematic parameters with the subscript d represent the desired values on the trajectory. These values are computed based on Table 2.2. The subscript a refers to the actual values of the kinematic parameters obtained by solving the control equations which involve the finite difference scheme and the relevant equations are Eq.(4.10), (4.11) and (4.12) mentioned in Section 4.3.1.

2. It should be noted that the desired values using Table 2.2 can be computed off-line based on the trajectory planning. On the other hand, the actual values and the errors etc., have to be computed on-line. One should try to minimize the on-line computations

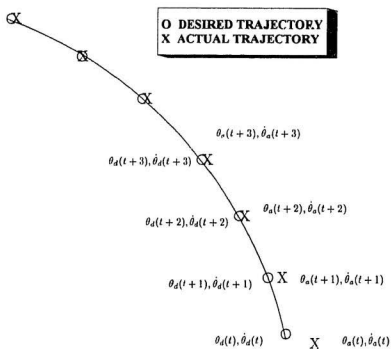


Figure 4.1 Specifications of the Desired and the Actual Trajectory

to increase the speed with which the task is performed.

3. $[K_p]$ and $[K_v]$ are diagonal matrices with diagonal elements consisting of position gain k_p and velocity gain k_v values respectively. Mathematically, they are written as

$$[K_p] = \begin{bmatrix} k_{p1} & 0 \\ 0 & k_{p2} \end{bmatrix} \text{ and } [K_v] = \begin{bmatrix} k_{v1} & 0 \\ 0 & k_{v2} \end{bmatrix} \quad (4.8)$$

The use of a single value respectively for the entire trajectory for k_p and k_v may not be able to produce torques to follow the desired trajectory. The trajectory control can be achieved by evaluating the set of gain parameters for the entire trajectory using non-linear optimization method (the optimal control method) as described in the Section 4.3.1 on a point by point basis. This requires the gain values to be different for each point along the trajectory of the manipulator. The objective of the optimal control is to minimize the errors in joint positions and joint velocities between the actual values and the desired values, based on the gain variables $[K_p]$ and $[K_v]$ as discussed below.

4.3.1. Evaluation of Gain Values Using Non-Linear Optimization Method

A simple planar two-link manipulator having two revolute joints shown in Fig.2.9 was considered. The trajectory involved with associated velocity profile are shown in Figs. 4.2 and 4.3 respectively. In Fig.4.3, the end effector accelerates from point A to

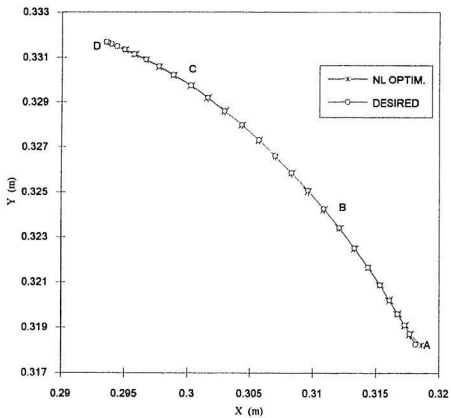


Figure 4.2 Desired Trajectory and the Trajectory Obtained Using Non-Linear Optimization Method

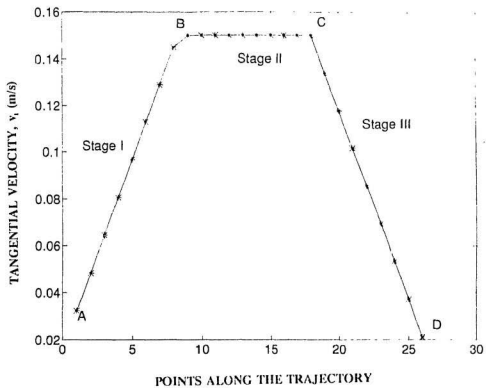


Figure 4.3 Desired Tangential Velocity Profile

Table 4.1 Various Parameters used for the Trajectory Control

	Link 1	Link 2
Link Lengths (m)	0.3	0.2
Mass (kg)	4.0	3.0
Radius of the Circle (m)	0.05	
Maximum Tangential Velocity v_t (m/s)	0.15	
Initial Position Gain Values	$k_{p1} = 100.5$; $k_{p2} = 200.10$;	
Initial Velocity Gain Values	$k_{v1} = 50.6$; $k_{v2} = 80.8$;	
Step value in time, Δt (s)	0.01	
Initial Position (rad)	$\Theta_1 = 1.1469$; $\Theta_2 = -0.9228$;	

point B (Stage I) and then traverses along the trajectory at constant tangential velocity v_t with 0.15 m/s (Stage II) to C and then decelerates to zero speed at D (Stage III). The various parameters used in the trajectory control are shown in Table 4.1. The variation of $\Theta_1, \Theta_2, \dot{\Theta}_1$ and $\dot{\Theta}_2$ of the desired trajectory are shown in Figs. 4.4 and 4.5 respectively.

The various steps involved (shown in Fig.4.6) are:

1. Note the link parameters like lengths, mass etc., (refer to Table 4.1).
2. Calculate the coordinates of the desired circular trajectory using (shown in Fig.2.22 with the specifications $\Theta_1 = 45^\circ, \Theta_2 = 0^\circ; r = 0.05$ m) a single variable α . The transformation matrices used were:

$$\begin{bmatrix} x \\ y \\ 0 \\ 1 \end{bmatrix} = \begin{bmatrix} \cos(\theta_1) & -\sin(\theta_1) & 0 & 1 \\ \sin(\theta_1) & \cos(\theta_1) & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \cos(\theta_2) & -\sin(\theta_2) & 0 & 1 \\ \sin(\theta_2) & \cos(\theta_2) & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \cos(\alpha) & -\sin(\alpha) & 0 & (d_2 + r) \\ \sin(\alpha) & \cos(\alpha) & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} r \\ 0 \\ 0 \\ 1 \end{bmatrix} \quad (4.9)$$

3. Calculate the joint parameters such as $\{\Theta_d(t)\}$ and the joint velocity vector $\{\dot{\Theta}_d(t)\}$ and joint acceleration $\{\ddot{\Theta}(t)\}$ for the desired trajectory using Eqs.(2.23) and (2.50) (corresponding to each point on the velocity profile). It can be done off line. Note the initial joint position $\{\Theta_s(t=0)\}$ and joint velocities $\{\dot{\Theta}_s(t=0)\}$ of the manipulator, and compute $\{e\}$ and $\{\dot{e}\}$ (shown in Figs. 4.7 and 4.8) mentioned in Eq.(4.7).

4. Compute the torque $\{\tau_e\}$ based on the error in joint position $\{e\}$ and joint velocity $\{\dot{e}\}$ using the Eq.(4.7). Substitute the torque in the dynamic equation, Eq.(4.6), and evaluate the joint acceleration $\{\ddot{\Theta}(t)\}$ using the expression:

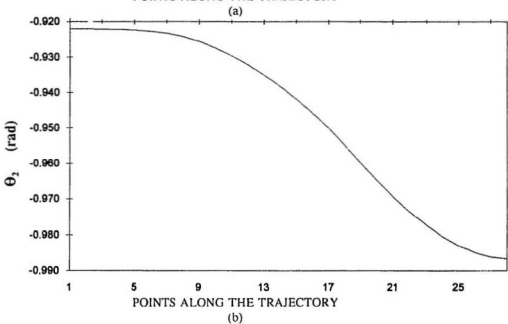
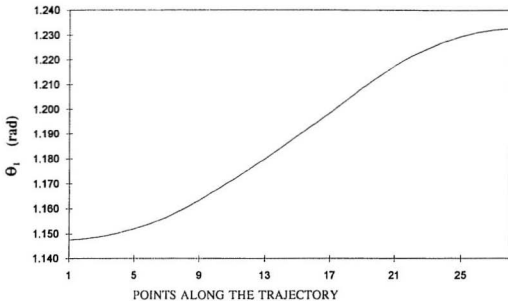


Figure 4.4 Variation of (a) θ_1 and (b) θ_2 Along the Desired Trajectory

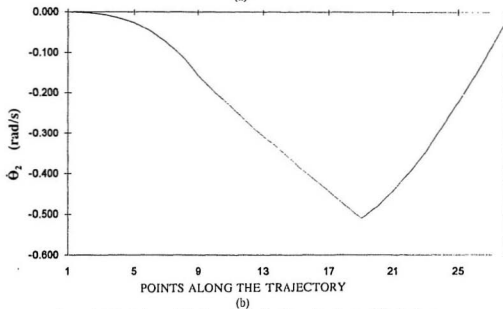
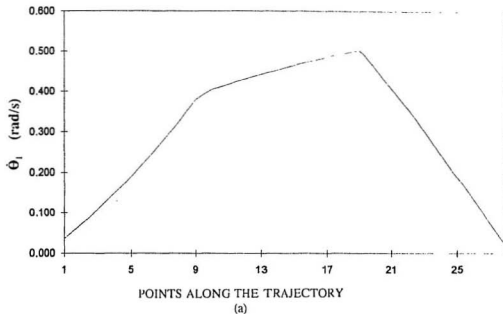


Figure 4.5 Variation of (a) $\dot{\theta}_1$ and (b) $\dot{\theta}_2$ Along the Desired Trajectory

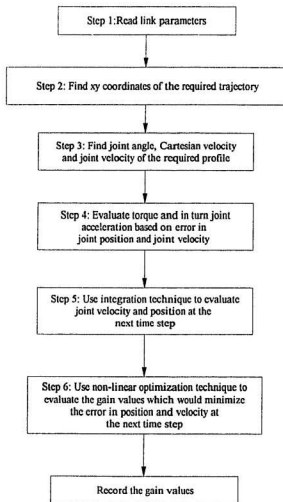


Figure 4.6 Flow Chart - Trajectory Control Using Non-Linear Optimization Method

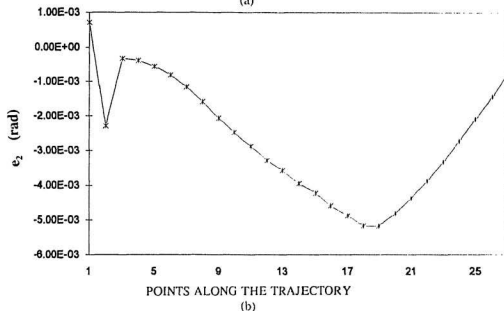
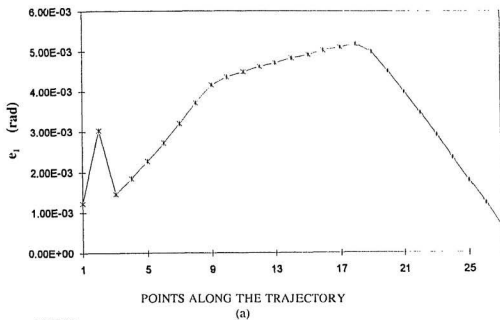
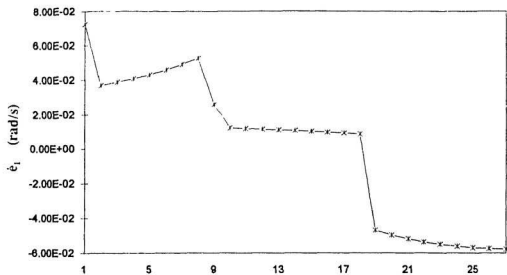
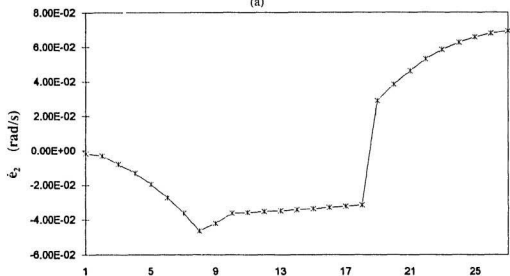


Figure 4.7 Variation of (a) e_1 and (b) e_2 Along the Trajectory



POINTS ALONG THE TRAJECTORY

(a)



POINTS ALONG THE TRAJECTORY

(b)

Figure 4.8 Variation of (a) \dot{e}_1 and (b) \dot{e}_2 Along the Trajectory

$$\{\ddot{\Theta}_a(t)\} = [M(\Theta_a(t))]^{-1} \{ \{\tau_r\} - \{V(\Theta_a(t), \dot{\Theta}_a(t))\} - \{G(\Theta_a(t))\} \} \quad (4.10)$$

5. Having calculated the joint accelerations, numerically integrate forward in steps of time Δt and obtain $\{\Theta_a(t+1)\}$ and $\{\dot{\Theta}_a(t+1)\}$ using Newmark- β scheme. The equations involved are:

$$\{\dot{\Theta}_a(t+1)\} = \{\dot{\Theta}_a(t)\} + [(1 - \beta) \{\ddot{\Theta}_a(t)\} + \beta \{\ddot{\Theta}_a(t+1)\}] \Delta t \quad (4.11)$$

$$\{\Theta_a(t+1)\} = \{\Theta_a(t)\} + \Delta t \{\dot{\Theta}_a(t)\} + [(0.5 - \alpha) \{\ddot{\Theta}_a(t)\} + \alpha \{\ddot{\Theta}_a(t+1)\}] \Delta t^2 \quad (4.12)$$

where α and β are known constants ($\alpha = 0.5$ and $\beta = 0.001$ were used in the present problem). The calculation of $\ddot{\Theta}^*(t+1)$ involves the following steps:

(a) Write an equation similar to Eq.(4.10) where the subscript a is replaced by d at time $t+1$. This can be mathematically expressed as:

$$\{\ddot{\Theta}^*(t+1)\} = [M(\Theta_d(t+1))]^{-1} \{ \{\tau^*\} - \{V(\Theta_d(t+1), \dot{\Theta}_d(t+1))\} - \{G(\Theta_d(t+1))\} \} \quad (4.13)$$

where

$$\{\tau^*\} = [K_p] \{ \Theta_d(t+2) - \Theta_d(t+1) \} + [K_v] \{ \dot{\Theta}_d(t+2) - \dot{\Theta}_d(t+1) \} \quad (4.14)$$

The computation of $\{\ddot{\Theta}^*(t+1)\}$ involves the quantities known at this step. There is no iteration required here.

6. The gain values are evaluated using non-linear optimization routine that would

minimize $\|\Theta_s(t+1) - \Theta_d(t+1)\|$ and $\|\dot{\Theta}_s(t+1) - \dot{\Theta}_d(t+1)\|$. Obtain $[K_p]$ and $[K_v]$ using the Hookes and Jeeves method (Rao, 1978) explained below:

Define

$$\{X\} = \begin{Bmatrix} k_{p1} \\ k_{p2} \\ k_{p3} \\ k_{p4} \end{Bmatrix}, \quad (4.15)$$

and

$$F(\{X\}) = \{\Theta_s(t+1) - \Theta_d(t+1)\}^2 + \{\dot{\Theta}_s(t+1) - \dot{\Theta}_d(t+1)\}^2 \quad (4.16)$$

The objective function can be mathematically written as

$$U(\{X\}) = F(\{X\}) + \sum_{k=1}^m P_k g_k^2 H(g_k) \quad (4.17)$$

where $\{X\}$ is the design vector and

k constraints are represented as g_k and

$H(g_k)$ is the Heavyside unit step function defined so that

$$\begin{aligned} H(g_k) &= 1 \quad \text{for } g_k \geq 0 \quad \text{or,} \\ H(g_k) &= 0 \quad \text{for } g_k < 0 \end{aligned} \quad (4.18)$$

In eq.(4.17), P_k are large penalty constants which are positive because the present problem is a minimization problem. Next, one needs to solve for the minimum of $U(\{X\})$ using the Hookes and Jeeves method and the step-by-step procedure for a design vector $\{X\}$ having n components is mentioned below:

(i) Start with an initial estimate of the design vector

$$\{X\} = \begin{Bmatrix} x_1 \\ x_2 \\ \vdots \\ x_n \end{Bmatrix} \quad (4.19)$$

and choose Δx_i , $i = 1, 2, \dots, n$ as step lengths in each of the coordinate directions u_i , $i = 1, 2, \dots, n$.

(ii) Set temporary base point $\{Y_{k,0}\} = \{X_k\}$

(iii) Start the exploratory move by perturbing one design variable at a time in order to find the improved value of the objective function. Set:

$$\begin{aligned} \{Y_{k,j}\} &= \begin{cases} \{Y_{k,j-1}\} + \Delta x_i \{u_i\} & \text{if } U^* = U(\{Y_{k,j-1}\} + \Delta x_i \{u_i\}) \\ & < U = U(\{Y_{k,j-1}\}) \\ \{Y_{k,j-1}\} - \Delta x_i \{u_i\} & \text{if } U = U(\{Y_{k,j-1}\} - \Delta x_i \{u_i\}) \\ & < U = U(\{Y_{k,j-1}\}) \\ \{Y_{k,j-1}\} & \text{if } U = U(\{Y_{k,j-1}\} + \Delta x_i \{u_i\}) \\ & < U^* = U(\{Y_{k,j-1}\} + \Delta x_i \{u_i\}) \end{cases} \\ \{Y_{k,j}\} &= \{Y_{k,j-1}\} \text{ if } U = U(\{Y_{k,j-1}\}) < \min(U^*, U) \end{aligned} \quad (4.20)$$

In this way, all the design variables x_n are perturbed and the improved position $\{Y_{k,n}\}$ found.

(iv) If the point $\{Y_{k,n}\}$ is not different from $\{X_k\}$, reduce the step lengths Δx_i ; set $i = 1$ and go to step (iii). If $\{Y_{k,n}\}$ is different from $\{X_k\}$ obtain the new base point as

$$\{X_{k+1}\} = \{Y_{k,n}\} \quad (4.21)$$

(v) Find the pattern direction $\{S\}$ using

$$\{S\} = \{X_{k+1}\} - \{X_k\} \quad (4.22)$$

Find the point $\{Y_{k+1,0}\}$ as

$$\{Y_{k+1,0}\} = \{X_{k+1}\} + \lambda \{S\} \quad (4.23)$$

Find λ^* , the optimum step length in the direction $\{S\}$ and use λ^* in Eq.(4.23).

(vi) Set $k = k+1$, $U_k = U(\{Y_{k,0}\})$ and $i = 1$; repeat step (iii). If at the end of step (iii), $U(\{Y_{k,n}\}) < U(X_k)$ use the new base point as $\{X_{k+1}\} = \{Y_{k,n}\}$ and go to step (v). If $U(\{Y_{k,n}\}) \geq U(\{X_k\})$, set $\{X_{k+1}\} = \{X_k\}$ and reduce step lengths; set $k = k+1$ and go to step (ii).

(vii) The process is terminated if the step lengths become less than ϵ , a very small quantity.

These gain values when substituted in Eq.(4.7) would result in the desired torque. The steps 3 to 6 were repeated for the entire trajectory and a set of gain values was obtained. The objective here was to have the position control primarily. The results in Fig.4.2 show that this objective was realized very well. The gain values for this trajectory are shown in Figs. 4.9 and 4.10 and the gain values change quite significantly along the trajectory. This is because the matrices $[M(\Theta)]$, $\{V(\Theta, \dot{\Theta})\}$ etc., undergo continuous change from position to position which also includes the changes in the velocity vector.

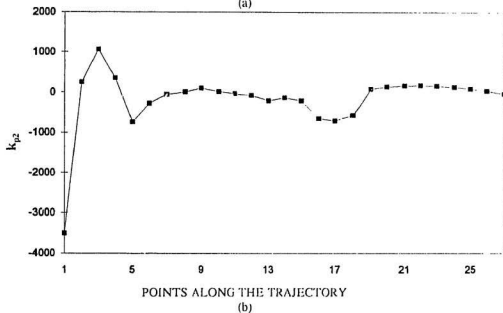
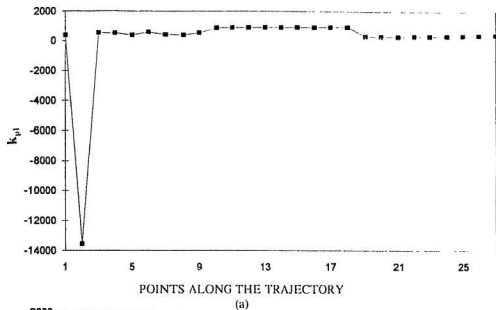


Figure 4.9 Variation of (a) k_{p1} and (b) k_{p2} Along the Trajectory

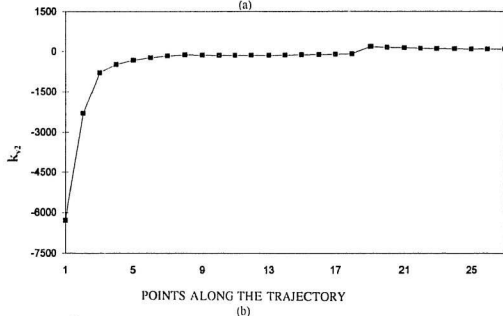
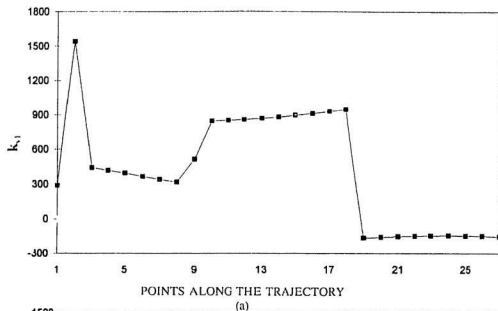


Figure 4.10 Variation of (a) k_{v1} and (b) k_{v2} Along the Trajectory

4.4 Neural Networks in Trajectory Control of Two-Link Manipulators

Neural network method has been widely used in many control applications. LP neuro method was found to be very effective in the mechanical design problems which was discussed in Chapter 3. It would be quite beneficial to have a weight matrix which relates the input vector

$$\{I\} = \{\theta_1, \theta_2, \dot{\theta}_1, \dot{\theta}_2, e_1, e_2, \dot{e}_1, \dot{e}_2\}^T \quad (4.24)$$

and the output vector

$$\{O\} = \{k_{p1}, k_{p2}, k_{v1}, k_{v2}\}^T \quad (4.25)$$

Several sets of $\{I\}$ and $\{O\}$ can be computed by starting with different initial conditions, but the same trajectory as shown in Figs. 4.2 and 4.3. Then the weight matrix $[W]$ can be obtained from these sets of $\{I\}$ and $\{O\}$ in accordance with the descriptions in Chapter 2. The problem of trajectory control computationally becomes a lot simpler now with the known weights $[W]$. The steps involved in obtaining the weight matrix as shown in Fig.4.11 are as follows:

Step 1: Let the end-effector be at some initial position having coordinates (x,y) .

Step 2: Use non-linear optimization method to evaluate gain values off-line for different trajectories.

Step 3: Note the input and output parameters for various trajectories.

Step 4: Compute $[W]$ using the LP-neuro method.

Step 5: Use $[W]$ on-line to evaluate the gain values (k_{p1} , k_{p2} etc .) as shown in Figs. 4.12 and 4.13. Here, the weight matrix relates the input and output vectors

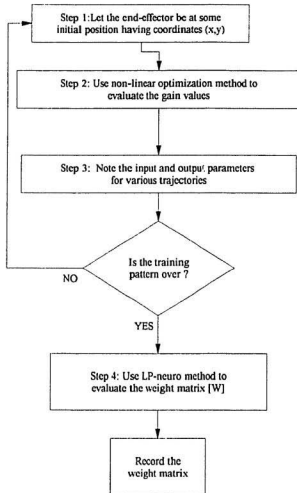
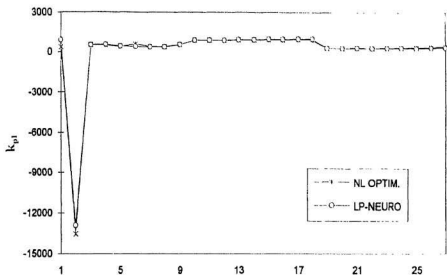
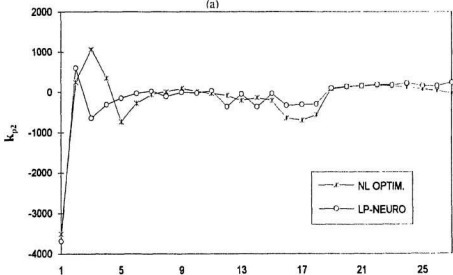


Figure 4.11 Flow Chart - Evaluation of Weight Matrix [W] for Trajectory Control Using LP-Neuro Method



POINTS ALONG THE TRAJECTORY

(a)



POINTS ALONG THE TRAJECTORY

(b)

Figure 4.12 Comparison of Gain Values (a) k_{p1} and (b) k_{p2} Obtained Using Non-Linear Optimization Method and LP-Neuro Method

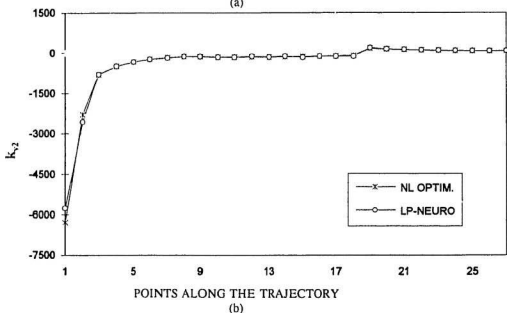
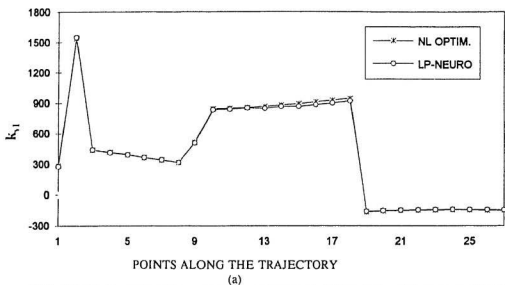


Figure 4.13 Comparison of Gain Values (a) k_{v1} and (b) k_{v2} Obtained Using Non-Linear Optimization Method and L2-Neuro Method

as

$$\begin{Bmatrix} k_{\rho 1} \\ k_{\rho 2} \\ k_{v1} \\ k_{v2} \end{Bmatrix} = [W] \begin{Bmatrix} \Theta_1 \\ \Theta_2 \\ \dot{\Theta}_1 \\ \dot{\Theta}_2 \\ e_1 \\ e_2 \\ \dot{e}_1 \\ \dot{e}_2 \end{Bmatrix} \quad (4.26)$$

The results corresponding to the steps mentioned above, carried out for the trajectory of a two-link manipulator, are shown in Fig. 4.14. These results clearly show the applicability of neural network method for on-line control of robotic manipulators.

4.5 Conclusions

Based on this work, the following conclusions can be drawn:

1. The non-linear control method yields accurate results.
2. LP-neuro method yields sufficiently accurate weight matrices for on-line control of robotic manipulators.

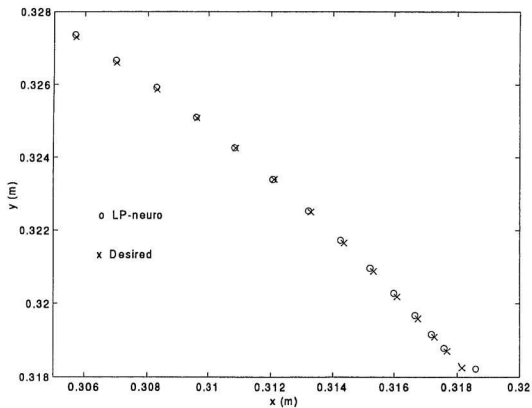


Figure 4.14 Desired Trajectory and the Trajectory Obtained Using LP-Neuro Method

Chapter 5

Conclusions

In this work, at first a new neural network learning algorithm called 'the LP-Neuro' method for obtaining the weights was developed. The problems in the design of mechanisms were solved using this method and the backpropagation method. After this, the gain values were obtained by optimal control technique in the case of robotic manipulators. These gain values were then used to compute the weights for the on-line control problems.

5.1 Conclusions

Based on this work, the following conclusions can be drawn:

1. Neural network method can be used in the velocity analysis of robotic manipulators near singular configurations, by establishing a mathematical relationship between the angular velocity and Cartesian velocity vectors.
2. In the inverse velocity analysis near singular configurations, the neural network method yielded more accurate results than the DLS method.
3. The neural network method established relationship over a segment of a trajectory rather than a point as in the case of the DLS method.

4. A new algorithm called LP-neuro method was developed in which elements of the weight matrix were formulated as the unknown variables of the LP problem.
5. The use of LP-neuro method resulted in faster convergence as compared to BP method in all cases.
6. One can successfully use the neural network technique to solve the mechanism design problems.
7. The non-linear optimization method was found successful in evaluating the set of gain values for the manipulator to follow the desired trajectory.
8. LP-neuro method can be used to evaluate the weight matrix $[W]$ that can be used in the on-line control of robotic manipulators.

5.2 Future Recommendations of the Work

Future research work can be pursued on the following topics:

1. LP-neuro method can be extended to many applications in the on-line control of robotic manipulators.
2. Efficient techniques like Karmarkar's algorithm can be applied in Linear Programming for faster convergence for problems involving large number of design variables.
3. It may be possible that the Optimal Control Method can be used in the on-line control of manipulators having more degrees of freedom if computations are done on parallel processors.

4. The neural network method can also be used to solve problems involving friction and other uncertainties in the trajectories of robotic manipulators.

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Appendix A: Program Listings

(All programs are written by the author)

A.1 Velocity Analysis near Singular Points

The Damped Least squares method, Psuedo-inverse method are implemented in the velocity analysis in this section. The input and output training vectors are obtained and the backpropagation algorithm is used to train the neural network. The analysis are carried out for a planar two-link manipulator (A.1.1) as well as PUMA-560 manipulator (A.1.2).

A.2 Acceleration Analysis of a Two-Link Manipulator

Acceleration analysis of a two-link manipulator are carried out and the neural network using backpropagation and LP-neuro method are used to train the network. The program **LP-Neuro** automatically forms coefficient matrix $[A]$ as well as the objective function according to Eq.(2.42).

A.3 Torque Analysis of a Two-Link Manipulator

Torque analysis is carried out using LP-neuro method as well as backpropagation method.

A.4 Nine-point Path Problem

LP-neuro method is used to train the network to design the four-bar mechanism based on several input-output training pattern.

A.5 Design of Four-Bar Function Generator

LP-neuro algorithm is again used to train the network to design a four-bar function generator.

A.6 Trajectory control of a Two-Link Manipulator

Variable gain values are obtained using a non-linear optimization routine and LP-neuro method is used to predict gain values based on error history in position and joint velocity. The weight matrix is used on-line to identify gain values for the required trajectory.

In general **OPTIVAR** - optimization library routine in (Siddall, 1982) is widely used for linear programming and non-linear optimization methods.

A.1 VELOCITY ANALYSIS NEAR SINGULAR POINTNS

NOTE: FOLLOWING ARE THE LIST OF FORTRAN CODES USED:
THESE CODES DO NOT BELONG TO A SINGLE FORTRAN PROGRAM.

A.1.1 Case 1: A Planar Two-link Manipulator

Step 1: Find the necessary cartesian coordinates, joint displacements, joint velocities of the desired trajectory.

Step 2: Prepare a database of input and output vector and train the neural network restraining the maximum joint velocity.

Step 3: Compare the joint velocity values obtained by the neural network method with the joint velocities obtained by psuedo-inverse method and SVD calculations.

```
C -----PROT2.FOR-----
C TO FIND THE CARTESIAN COORDINATES OF THE
C DESIRED TRAJECTORY
C STRAIGHT LINE PART OF THE TRAJECTORY
C TWO D.O.F - PLANAR TWO LINK MANIPULATOR
C IMPLICIT REAL*8(A-H,O-Z)
C INTRINSIC DATAN2D,DCOSD,DSIND
C DIMENSION R(3,3),XP(3),X(3),DT(3),VDT(3)
C OPEN(1, FILE = 'PROT2.DAT' , STATUS = 'OLD')
C OPEN(2, FILE = 'XY.MAT', STATUS = 'NEW' )
C OPEN(3, FILE = 'VEL.MAT', STATUS = 'NEW' )
C OPEN(4, FILE = 'PHI.MAT', STATUS = 'NEW' )
C OPEN(5, FILE = 'SLOPE.MAT', STATUS = 'NEW')
C OPEN(6, FILE = 'PFDIST.MAT', STATUS = 'NEW')
C OPEN(7, FILE = 'DIST.MAT', STATUS = 'NEW')
C *****
C READ(1,*)VEL
C READ(1,*)RADIUS
C READ(1,*)ORANG
C READ(1,*)ITER
C READ(1,*)STAR2
C READ(1,*)STEP2
C XO = 0.530D0 * DCOSD(ORANG)
C YO = 0.530D0 * DSIND(ORANG)
C *****
C DO 110 NO = 1,ITER
```

```

R(1,1) = DCOSD(ORANG)
R(1,2) = -DSIND(ORANG)
R(1,3) = XO
R(2,1) = DSIND(ORANG)
R(2,2) = DCOSD(ORANG)
R(2,3) = YO
R(3,1) = 0.0D0
R(3,2) = 0.0D0
R(3,3) = 1.0D0
XP(1) = (RADIUS - STAR2)
XP(2) = 0.0D0
XP(3) = 1.0D0
DIST = DIST + STEP2
WRITE(7,*)DIST
WRITE(4,*)STAR2
CALL RMATVEC(R,XP,X)
WRITE(2,*)X(1),X(2)
C *****
DT(1) = VEL
DT(2) = 0.0D0
DT(3) = 0.0D0
CALL RMATVEC(R,DT,VDT)
WRITE(3,*)VDT(1),VDT(2)
DO 120 I = 1,3
XP(I) = 0.0D0
X(I) = 0.0D0
DO 120 J = 1,3
R(I,J) = 0.0D0
120 CONTINUE
STAR2 = STAR2 + STEP2
110 CONTINUE
WRITE(6,*)DIST
STOP
END

SUBROUTINE RMATVEC(A,B,C)
IMPLICIT REAL*8(A-H,O-Z)
DIMENSION A(3,3),B(3),C(3)
DO 30 I = 1,3
C(I) = 0.0D0
DO 40 J = 1,3
C(I) = C(I) + A(I,J) * B(J)
40 CONTINUE
30 CONTINUE

```

```

RETURN
END

```

```

C -----PROT1.FOR-----
C TO FIND THE CARTESIAN COORDINATES OF THE
C DESIRED TRAJECTORY
C ARC PART OF THE PROJECTORY
C TWO D.O.F - PLANAR TWO LINK MANIPULATOR
IMPLICIT REAL*8(A-H,O-Z)
INTRINSIC DATAN2D,DCOSD,DSIND
DIMENSION R(3,3),XP(3),X(3),DT(3),VDT(3)
OPEN(1, FILE = 'PROT1.DAT', STATUS = 'OLD')
OPEN(2, FILE = 'XY.MAT', STATUS = 'NEW')
OPEN(3, FILE = 'VEL.MAT', STATUS = 'NEW')
OPEN(4, FILE = 'PHI.MAT', STATUS = 'NEW')
OPEN(5, FILE = 'SLOPE.MAT', STATUS = 'NEW')
OPEN(6, FILE = 'PFDIST.MAT', STATUS = 'OLD')
OPEN(7, FILE = 'DIST.MAT', STATUS = 'NEW')
C *****
PI = 3.141592654D0
READ(1,*)VEL
READ(1,*)RADIUS
READ(1,*)ORANG
READ(1,*)ITER
READ(1,*)STAR1
READ(1,*)STEP1
READ(6,*)PFD
XO = 0.530D0 * DCOSD(ORANG)
YO = 0.530D0 * DSIND(ORANG)
C *****
DO 10 NO = 1,ITER
R(1,1) = DCOSD(ORANG)
R(1,2) = -DSIND(ORANG)
R(1,3) = XO
R(2,1) = DSIND(ORANG)
R(2,2) = DCOSD(ORANG)
R(2,3) = YO
R(3,1) = 0.0D0
R(3,2) = 0.0D0
R(3,3) = 1.0D0
XP(1) = RADIUS * DCOSD(STAR1)
XP(2) = RADIUS * DSIND(STAR1)
XP(3) = 1.0D0

```

```

DIST = (PI/180.0D0)*(STEP1)*RAD!US*REAL(NO) + PFD
WRITE(4,*)STAR1
WRITE(7,*)DIST
CALL RMATVEC(R,XP,X)
WRITE(2,*)X(1),X(2)
PR1 = XP(2)
PR2 = -XP(1)
ANG = DATAN2D(PR2,PR1)
C *****
WRITE(5,*)ANG
DT(1) = VEL * DCOSD(ANG)
DT(2) = VEL * DSIND(ANG)
DT(3) = 0.0D0
CALL RMATVEC(R,DT,VDT)
WRITE(3,*)VDT(1),VDT(2)
DO 20 I = 1,3
XP(I) = 0.0D0
X(I) = 0.0D0
DO 20 J = 1,3
P(I,J) = 0.0D0
20 CONTINUE
STAR1 = STAR1 + STEP1
10 CONTINUE
C *****
STOP
END

C -----ANGFIND.FOR-----
C TO FIND THE JOINT DISPLACEMENTS
C FOR A TWO DOF PLANAR MANIPULATOR
IMPLICIT REAL*8(A-H,O-Z)
INTRINSIC DATAN2D
OPEN(1, FILE = 'ANGFIND.DAT', STATUS = 'OLD')
OPEN(2, FILE = 'XY.MAT', STATUS = 'OLD')
OPEN(3, FILE = 'THETA.MAT', STATUS = 'NEW')
OPEN(4, FILE = 'ANOTHETA.MAT', STATUS = 'NEW')
C *****
READ(1,*)RL1,RL2
READ(1,*)ITER
DO 10 NO = 1,ITER
READ(2,*)XO,YO
T = 0.0D0
RJ = 2. * YO * RL1
RI = 2. * XO * RL1

```

```

RK = YO*YO + XO*XO + RL1*RL1 - RL2*RL2
T = (RJ*RJ) + (RI * RI) - (RK*RK)
ALPHA1 = DATAN2D(RJ,RJ)+DATAN2D(DSQR(T),RK)
ALPHA2 = DATAN2D(RJ,RI)+DATAN2D(-DSQR(T),RK)
BETA1 = DATAN2D((YO-RL1*DSIND(ALPHA1)))-ALPHA1
% (XO-RL1*DCOSD(ALPHA1)))-ALPHA1
BETA2 = DATAN2D((YO-RL1*DSIND(ALPHA2)))-ALPHA2
% (XO-RL1*DCOSD(ALPHA2)))-ALPHA2
WRITE(3,*) ALPHA1,BETA1
WRITE(4,*)ALPHA1,BETA1
WRITE(4,*)ALPHA2,BETA2
WRITE(4,*)
10  CONTINUE
STOP
END

C -----TDTFIND.FOR-----
C TO FIND JOINT VELOCITY
C INVERSE KINEMATICS FOR TWO D.O.F PLANAR MANIPULATOR
IMPLICIT REAL*8(A-H,O-Z)
INTRINSIC DATAN2D,DCOSD,DSIND
DIMENSION VEL(2),THETA(2),RJ(2,2),RJINV(2,2),TDOT(2)
OPEN(1, FILE = 'TDTFIND.DAT', STATUS = 'OLD')
OPEN(2, FILE = 'THETA.MAT', STATUS = 'OLD')
OPEN(3, FILE = 'VEL.MAT', STATUS = 'OLD')
OPEN(4, FILE = 'DETER.MAT', STATUS = 'NEW')
OPEN(5, FILE = 'THETADT.MAT', STATUS = 'NEW')
OPEN(6, FILE = 'JACOBIAN.MAT', STATUS = 'NEW')
C *****
READ(1,*)RL1,RL2
READ(1,*)ITER
DO 10 NO = 1,ITER
READ(2,*)THETA(1),THETA(2)
READ(3,*)VEL(1),VEL(2)
RJ(1,1) = -RL1*DSIND(THETA(1)) - RL2*DSIND(THETA(1) +
* THETA(2))
RJ(1,2) = -RL2*DSIND(THETA(1) + THETA(2))
RJ(2,1) = RL1*DCOSD(THETA(1)) + RL2*DCOSD(THETA(1) +
* THETA(2))
RJ(2,2) = RL2*DCOSD(THETA(1) + THETA(2))
DO 15 II = 1,2
WRITE(6,*)(RJ(II,JJ),JJ=1,2)
15  CONTINUE
DETER = RL1*RL2*DSIND(THETA(2))

```

```

WRITE(4,*)DETER
RJINV(1,1) = RJ(2,2)/DETER
RJINV(1,2) = -RJ(1,2)/DETER
RJINV(2,1) = -RJ(2,1)/DETER
RJINV(2,2) = RJ(1,1)/DETER
CALL RMATVEC(RJINV,VEL,TDOT)
WRITE(5,*)TDOT(1),TDOT(2)
DO 20 I = 1,2
  VEL(I) = 0.0D0
  THETA(I) = 0.0D0
  TDOT(I) = 0.0D0
DO 30 J = 1,2
  RJ(I,J) = 0.0D0
  RJINV(I,J) = 0.0D0
30  CONTINUE
20  CONTINUE
10  CONTINUE
STOP
END

C -----MAX.FOR-----
C TO FIND THE MAXIMUM AND MINIMUM OF JOINT VELOCITIES
IMPLICIT REAL*8(A-H,O-Z)
DIMENSION TDOT1(100),TDOT2(100)
OPEN(1, FILE= 'THETADT.MAT', STATUS='OLD')
OPEN(2, FILE= 'SDOT.MAT', STATUS='NEW')
READ(*,*)NO
DO 10 I = 1, NO
  READ(1,*)TDOT1(I),TDOT2(I)
10  CONTINUE
CALL MINMAX(TDOT1,SMALL1,PLARGE1,NO)
CALL MINMAX(TDOT2,SMALL2,PLARGE2,NO)
DO 20 I = 1,NO
  SDOT1 = (TDOT1(I) - SMALL1)/(PLARGE1 - SMALL1)
  SDOT2 = (TDOT2(I) - SMALL2)/(PLARGE2 - SMALL2)
  WRITE(2,*)SDOT1,SDOT2
20  CONTINUE
STOP
END

SUBROUTINE MINMAX(A,B,C,NO)
IMPLICIT REAL*8(A-H,O-Z)
DIMENSION A(100)

```

```

C      INITIALIZE THE SMALLEST AND LARGEST AS THE FIRST ENTRY
      SMALL = A(1)
      PLARGE = A(1)
C      SEARCH THE REST OF THE ARRAY FOR BETTER VALUES
      DO 100 I = 2,NO
        IF(A(I).LT.SMALL) THEN
          SMALL = A(I)
        ELSE
          IF (A(I).GT.PLARGE) THEN
            PLARGE = A(I)
          ENDIF
        ENDIF
100    CONTINUE
      B = SMALL
      C = PLARGE
      RETURN
      END

C      -----NURAL.FOR-----
C      A NEURAL NET PROGRAM (BACK PROPOGATION ALGORITHM)
C      *****
C      VELOCITY ANALYSIS OF TWO-LINK MANIPULATOR
C      *****
      IMPLICIT REAL*8(A-H,O-Z)
      INTRINSIC DEXP
      DIMENSION V(20,20),W(20,20)
      DIMENSION XDOT(100),YDOT(100),ZDOT(100)
      DIMENSION TDOT1(100),TDOT2(100),TDOT3(100)
      DIMENSION DTDOT1(100),DTDOT2(100),DTDOT3(100)
      DIMENSION RI(100),RM(100),RO(100)
      DIMENSION
%      FRM(100),FRO(100),FTDOT1(100),FTDOT2(100),FTDOT3(100)
      DIMENSION FRMD(100),FROD(100)
      DIMENSION EOS(100),EMS(100)
      OPEN(1, FILE='NURAL.DAT', STATUS='OLD')
      OPEN(3, FILE='VEL.MAT', STATUS='OLD')
      OPEN(4, FILE='ALPHA.MAT', STATUS='NEW')
      OPEN(5, FILE='BETA.MAT', STATUS='NEW')
C      *****
C      ENTER NO. OF INPUT,MIDDLE AND OUTPUT LAYER NEURONS
      READ(1,*)INNO
      READ(1,*)MIDNO
      READ(1,*)NOUTNO
C      ENTER NO. OF INPUT TRAINING DATAS

```

```

      READ(1,*)NODATA
C     ENTER NO. OF ITERATIONS
      READ(1,*)ITER
C     ENTER THE LEARNING RATE
      READ(1,*)ETA
C     *****
C     READ THE TRAINING INPUT VALUES & THEIR CORRESPONDING
C     OUTPUT VALUES
      DO 10 I = 1,NODATA
      READ(2,*)TDOT1(I),TDOT2(I)
      READ(3,*)XDOT(I),YDOT(I)
      FTDOT1(I) = (1.0D0/(1.0D0 + DEXP(-TDOT1(I))))
      FTDOT2(I) = (1.0D0/(1.0D0 + DEXP(-TDOT2(I))))
10    CONTINUE
C     *****
C     RANDOM NUMBER GENERATION FOR INITIAL INPUT AND
C     OUTPUT WEIGHT MATRICES
C     *****
C     SEED FOR RANDOM NUMBER GENERATOR
      ISEED = 23148
      JSEED = 32124
      DO 20 I = 1,MIDNO
      DO 20 J = 1,INNO
      RV = RAN(ISEED)*2.0D0 - 1.0D0
      V(I,J) = RV
20    CONTINUE
      DO 30 I = 1,NOUTNO
      DO 30 J = 1,MIDNO
      RW = RAN(JSEED)*2.0D0 - 1.0D0
30    CONTINUE
C     *****
C     TRAINING STARTS HERE
C     *****
      DO 40 NO = 1,ITER
C     *****
      DO 50 KD = 1,NODATA
      RI(1) = XDOT(KD)
      RI(2) = YDOT(KD)
      DO 60 KR = 1,MIDNO
      RM(KR) = 0.0D0
      DO 70 KP = 1,INNO
      RM(KR) = RM(KR) + V(KR,KP)*RI(KP)
70    CONTINUE
      FRM(KR) = (1.0D0/(1.0D0 + DEXP(-RM(KR))))

```



```

FRMD(KR) = FRM(KR)*(1.0D0 - FRM(KR))
60  CONTINUE
    DO 80 KR = 1,NOUTNO
        RO(KR) = 0.0D0
        DO 90 KP = 1,MIDNO
            RO(KR) = RO(KR) + W(KR,KP)*FRM(KP)
90  CONTINUE
        FRO(KR) = (1.0D0/(1.0D0 + DEXP(-RO(KR))))
        FROD(KR) = FRO(KR)*(1.0D0 - FRO(KR))
80  CONTINUE
C *****
C  ERROR UPDATE
C *****
    DO 100 J = 1,MIDNO
        EMS(J) = 0.0D0
100 CONTINUE
        EOS(1) = FTDOT1(KD) - FRO(1)
        EOS(2) = FTDOT2(KD) - FRO(2)
        DO 110 IE = 1,NOUTNO
            DO 120 JE = 1,MIDNO
                EMS(JE) = EMS(JE) + EOS(IE)*FROD(IE)*W(IE,JE)
120 CONTINUE
110 CONTINUE
C *****
C  WEIGHT UPDATE
C *****
    DO 200 IRT = 1,NOUTNO
        DO 210 JRT = 1,MIDNO
            W(IRT,JRT) = W(IRT,JRT) + ETA*EOS(IRT)*FROD(IRT)*FRM(JRT)
210 CONTINUE
200 CONTINUE
        DO 220 IRT = 1,MIDNO
            DO 230 JRT = 1,INNO
                V(IRT,JRT) = V(IRT,JRT) + ETA*EMS(IRT)*FRMD(IRT)*RI(JRT)
230 CONTINUE
220 CONTINUE
C *****
    DO 300 I = 1,MIDNO
        RM(I) = 0.0D0
        DO 310 J = 1,INNO
            RM(I) = RM(I) + V(I,J)*RI(J)
310 CONTINUE
        FRM(I) = (1.0D0/(1.0D0 + DEXP(-RM(I))))
300 CONTINUE

```

```

DO 320 I = 1,NOUTNO
RO(I) = 0.0D0
DO 330 J = 1,MIDNO
RO(I) = RO(I) + W(I,J)*FRM(J)
330 CONTINUE
320 CONTINUE
C *****
C FINAL OUTPUT AT THE END OF EACH ITERATION
C *****
DTDOT1(KD) = RO(1)
DTDOT2(KD) = RO(2)
50 CONTINUE
40 CONTINUE
C *****
C COMPARISON OF NEURAL AND ACTUAL OUTPUT
C *****
DO 500 IT = 1,NODATA
WRITE(4,*)DTDOT1(IT),TDOT1(IT)
WRITE(5,*)DTDOT2(IT),TDOT2(IT)
500 CONTINUE
STOP
END

c -----REBAK.FOR-----
C TO FIND THE MAGNITUDE OF THE ERROR
IMPLICIT REAL*8(A-H,O-Z)
DIMENSION TDOT1(100),TDOT2(100)
DIMENSION DTDOT1(100),DTDOT2(100)
OPEN(1, FILE= 'THETADT.MAT', STATUS='OLD')
OPEN(3, FILE= 'ALPHA.MAT', STATUS='OLD')
OPEN(4, FILE= 'BETA.MAT', STATUS='OLD')
OPEN(6, FILE= 'REBAK.MAT', STATUS='NEW')
OPEN(7, FILE= 'RERR.MAT', STATUS='NEW')
READ(*,*)NO
DO 10 I = 1, NO
READ(1,*)TDOT1(I),TDOT2(I)
READ(3,*)DTDOT1(I)
READ(4,*)DTDOT2(I)
10 CONTINUE
CALL MINMAX(TDOT1,SMALL1,PLARGE1,NO)
CALL MINMAX(TDOT2,SMALL2,PLARGE2,NO)
DO 20 I = 1,NO
SDOT1 = DTDOT1(I)*(PLARGE1 - SMALL1) + SMALL1
SDOT2 = DTDOT2(I)*(PLARGE2 - SMALL2) + SMALL2

```

```

WRITE(6,*)SDOT1,SDOT2
C   TO FIND OUT THE MAGNITUDE OF ERROR
   UPP = TDOT1(I) - SDOT1
   VPP = TDOT2(I) - SDOT2
   ERR = SQRT(UPP*UPP + VPP*VPP)
   WRITE(7,*)ERR
20  CONTINUE
   STOP
   END

C   -----PSUD.FOR-----
C   PSEUDO-INVERSE SOLUTION OF A TWO-LINK MANIPULATOR
C   NEAR SINGULARITIES
   IMPLICIT REAL*8(A-H,O-Z)
   PARAMETER (NRA=2,NCA=2,LDA=NRA,LDGINV=NCA)
   DIMENSION A(LDA,NCA),AINV(LDGINV,NRA)
   DIMENSION V(2),PST(2)
   OPEN(1, FILE = 'JACOBIAN.MAT', STATUS = 'OLD')
   OPEN(2, FILE = 'VEL.MAT', STATUS = 'OLD')
   OPEN(3, FILE = 'PSTETA.MAT', STATUS = 'NEW')
   WRITE(*,*)'NO OF DATAS ?'
   READ(*,*)ITER
   DO 10 NO = 1,ITER
   DO 20 I = 1,NRA
   READ(1,*)(A(I,J),J=1,NCA)
20  CONTINUE
   READ(2,*)V(1),V(2)
   TOL = 10.0 * AMACH(4)
C   *****
C   CALLING IMSL ROUTINE FOR PSUEDO-INVERSE
C   *****
   CALL DLSGRR(NRA,NCA,A,LDA,TOL,IRANK,AINV,LDGINV)
   CALL RMAVECC(AINV,V,PST)
   WRITE(3,*)PST(1),PST(2)
10  CONTINUE
   STOP
   END

C   -----IYO.FOR-----
C   COMPARISON OF THE VALUES AND PRINTING THE RESULTS
   IMPLICIT REAL*8(A-H,O-Z)
   INTRINSIC DSQRT
   DIMENSION ALPHA(2),BETA(2),GAMMA(2)
   OPEN(1, FILE = 'THETADT.MAT', STATUS = 'OLD')

```

```

OPEN(2, FILE = 'REBAK.MAT', STATUS = 'OLD')
OPEN(5, FILE = 'PSTETA.MAT', STATUS = 'OLD')
OPEN(3, FILE = 'SNORM.MAT', STATUS = 'NEW')
OPEN(4, FILE = 'PHI.MAT', STATUS = 'OLD')
WRITE(*,*)'ITERATIONS ? '
READ(*,*)ITER
DO 10 NO = 1,ITER
  READ(1,*)ALPHA(1),BETA(1)
  READ(2,*)ALPHA(2),BETA(2)
  READ(5,*)GAMMA(1),GAMMA(2)
  READ(4,*)PHI
  TSQP = DSQRT(ALPHA(1)*ALPHA(1) + BETA(1)*BETA(1))
  SQP = DSQRT(ALPHA(2)*ALPHA(2)+BETA(2)*BETA(2))
  PERT = DSQRT(GAMMA(1)*GAMMA(1)+GAMMA(2)*GAMMA(2))
  WRITE(3,*)TSQP,SQP,PERT
10 CONTINUE
STOP
END

```

A.1.2 Case 2: Puma-560 Manipulator

Step 1: Find the necessary cartesian coordinates, joint displacements, joint velocities of the desired trajectory.

Step 2: Prepare a database of input and output vector and train the neural network restraining the maximum joint velocity.

Step 3: Compare the joint velocity values obtained by the neural network method with the joint velocities obtained by psuedo-inverse method and SVD calculations.

```

C *****
IMPLICIT REAL*8(A-H,O-Z)
OPEN(UNIT=1,FILE='RANG.MAT',STATUS='NEW')
WRITE(*,*)'NO. OF DATAS'
READ(*,*)NO
WRITE(*,*)'INITIAL THETA3 ?'
READ(*,*)T3
WRITE(*,*)'INCREMENTAL THETA3 ?'
READ(*,*)DELT
T1 = 0.0D0
T2 = -1.90843D0

```

```

DO 10 I = 1,NO
T3 = T3 + DELT
WRITE(1,*)T1,T2,T3
10 CONTINUE
STOP
END

C *****
C TO GENERATE CARTESIAN COORDINATES
C FOR THE CIRCULAR TRAJECTORY
C *****
IMPLICIT REAL*8(A-H,O-Z)
INTRINSIC DSIND,DCOSD
EXTERNAL DMURRV
DIMENSION TRA(4,4),P3(4),XYZ(4)
OPEN(UNIT=1,FILE='RANG.MAT',STATUS='OLD')
OPEN(UNIT=2,FILE='PUMA.DAT',STATUS='OLD')
OPEN(UNIT=3,FILE='COORD.MAT',STATUS='NEW')
READ(2,*)A2,A3,D3,D4
WRITE(*,*)'NO OF DATAS ? '
READ(*,*)ITER
DO 10 I = 1,ITER
READ(1,*)T1,T2,T3
C1 = DCOSD(T1)
S1 = DSIND(T1)
C2 = DCOSD(T2)
S2 = DSIND(T2)
C23 = DCOSD(T2+T3)
S23 = DSIND(T2+T3)
TRA(1,1) = C1*C23
TRA(1,2) = -C1*S23
TRA(1,3) = -S1
TRA(1,4) = C1*A2*C2 - S1*D3
TRA(2,1) = S1*C23
TRA(2,2) = -S1*S23
TRA(2,3) = C1
TRA(2,4) = S1*A2*C2 + C1*D3
TRA(3,1) = -S23
TRA(3,2) = -C23
TRA(3,3) = 0.0D0
TRA(3,4) = -A2*S2
TRA(4,1) = 0.0D0
TRA(4,2) = 0.0D0
TRA(4,3) = 0.0D0

```

```

TRA(4,4) = 1.0D0
P3(1) = A3
P3(2) = D4
P3(3) = 0.0D0
P3(4) = 1.0D0
CALL DMURRV(4,4,TRA,4,4,P3,1,4,XYZ)
WRITE(3,*)XYZ(1),XYZ(2),XYZ(3)
10  CONTINUE
    STOP
    END

C *****
C  A PROGRAM FOR GENERATING THE CARTESIAN VELOCITIES
C  FOR A PUMA-560 MANIPULATOR
C *****
IMPLICIT REAL*8(A-H,O-Z)
INTRINSIC DATAN2D,DSIND,DCOSD
OPEN(UNIT=1,FILE='PUMA.DAT',STATUS='OLD')
OPEN(UNIT=3,FILE='PUMAVEL.MAT',STATUS='NEW')
OPEN(UNIT=4,FILE='COORD.MAT',STATUS='OLD')
READ(1,*)A2,A3,D3,D4
WRITE(*,*)'NO OF DATAS ?'
READ(*,*)NO
VELOCITY = 0.03D0
DO 10 I = 1,NO
  READ(4,*)X,Y,Z
  SL1 = A2 - X
  SL2 = Z
  SLOPE = DATAN2D(SL1,SL2)
  VX = VELOCITY * DCOSD(SLOPE)
  VY = 0.0D0
  VZ = VELOCITY * DCOSD(270.0D0+SLOPE)
  WRITE(3,*)VX,VY,VZ
10  CONTINUE
    STOP
    END

C *****
C  A PROGRAM FOR GENERATING THE CARTESIAN VELOCITIES FOR
C  A PUMA-560 MANIPULATOR
C *****
IMPLICIT REAL*8(A-H,O-Z)

```

```

INTRINSIC DATAN2D,DSIND,DCOSD
DIMENSION RJ(3,3),VEL(3),THDT(3),RJINV(3,3)
DIMENSION FTHDT(3)
OPEN(UNIT=1,FILE='PUMA.DAT',STATUS='OLD')
OPEN(UNIT=2,FILE='RANG.MAT',STATUS='OLD')
OPEN(UNIT=3,FILE='PUMAVEL.MAT',STATUS='OLD')
OPEN(UNIT=5,FILE='TDOT.DAT',STATUS='NEW')
OPEN(UNIT=6,FILE='DETER.MAT',STATUS='NEW')
READ(1,*)A2,A3,D3,D4
WRITE(*,*)'NO OF DATAS ?'
READ(*,*)NO
DO 43 I = 1,NO
READ(2,*)T1,T2,T3
S1 = DSIND(T1)
S2 = DSIND(T2)
C1 = DCOSD(T1)
C2 = DCOSD(T2)
C23 = DCOSD(T2+T3)
S23 = DSIND(T2+T3)
RJ(1,1) = -A3*S1*C23 + D4*S1*S23 - A2*C2*S1 - D3*C1
RJ(1,2) = -A3*C1*S23 - D4*C1*C23 - A2*S2*C1
RJ(1,3) = -A3*C1*S23 - D4*C1*C23
RJ(2,1) = A3*C1*C23 - D4*C1*S23 + A2*C2*C1 - D3*S1
RJ(2,2) = -A3*S1*S23 - D4*S1*C23 - A2*S2*S1
RJ(2,3) = -A3*S1*S23 - D4*S1*C23
RJ(3,1) = 0.0D0
RJ(3,2) = -A3*C23 + D4*S23 - A2*C2
RJ(3,3) = -A3*C23 + D4*S23
*****
C      COMPUTE THE DETERMINANT OF JACOBIAN
C      *****
XT1 = RJ(2,2)*RJ(3,3) - RJ(3,2)*RJ(2,3)
XT2 = RJ(2,1)*RJ(3,3) - RJ(3,1)*RJ(2,3)
XT3 = RJ(2,1)*RJ(3,2) - RJ(3,1)*RJ(2,2)
DETER = RJ(1,1)*XT1 - RJ(1,2)*XT2 + RJ(1,3)*XT3
WRITE(6,*)DETER
CALL DLINRG(3,RJ,3,RJINV,3)
READ(3,*)VEL(1),VEL(2),VEL(3)
CALL DMURRV(3,3,RJINV,3,3,VEL,1,3,FTHDT)
WRITE(5,*)FTHDT(1),FTHDT(2),FTHDT(3)
DO 50 INK = 1,3
DO 50 JNK = 1,3
RJ(INK,JNK) = 0.0D0
RJINV(INK,JNK) = 0.0D0

```

```

50  CONTINUE
43  CONTINUE
    STOP
    END

    IMPLICIT REAL*8(A-H,O-Z)
    DIMENSION TDOT1(100),TDOT2(100),TDOT3(100)
    OPEN(UNIT=1,FILE='TDOT.MAT',STATUS='OLD')
    OPEN(UNIT=2,FILE='SDOT.MAT',STATUS='NEW')
    READ(*,*)NO
    DO 10 I = 1, NO
    READ(1,*)TDOT1(I),TDOT2(I),TDOT3(I)
10  CONTINUE
    CALL MINMAX(TDOT2,SMALL2,PLARGE2,NO)
    CALL MINMAX(TDOT3,SMALL3,PLARGE3,NO)
    DO 20 I = 1,NO
c   SDOT1 = (TDOT1(I) - SMALL1)/(PLARGE1 - SMALL1)
    SDOT2 = (TDOT2(I) - SMALL2)/(PLARGE2 - SMALL2)
    SDOT3 = (TDOT3(I) - SMALL3)/(PLARGE3 - SMALL3)
    WRITE(2,*)SDOT1,SDOT2,SDOT3
20  CONTINUE
    STOP
    END

C   A NEURAL NET PROGRAM (BACK-PROPAGATION ALGORITHM)
C   *****
C   VELOCITY ANALYSIS OF PUMA-560 MANIPULATOR
C   *****
    IMPLICIT REAL*8(A-H,O-Z)
    INTRINSIC DEXP
    DIMENSION V(20,20),W(20,20)
    DIMENSION XDOT(100),YDOT(100),ZDOT(100)
    DIMENSION TDOT1(100),TDOT2(100),TDOT3(100)
    DIMENSION DTDOT1(100),DTDOT2(100),DTDOT3(100)
    DIMENSION RI(100),RM(100),RO(100)
    DIMENSION
%   FRM(100),FRO(100),FTDOT1(100),FTDOT2(100),FTDOT3(100)
    DIMENSION FRMD(100),FROD(100)
    DIMENSION EOS(100),EMS(100)
    OPEN(UNIT=1,FILE='RAKO.DAT',STATUS='OLD')
    OPEN(UNIT=2,FILE='SDOT.MAT',STATUS='OLD')
    OPEN(UNIT=3,FILE='PUMAVEL.MAT',STATUS='OLD')
    OPEN(UNIT=4,FILE='ALPHA.MAT',STATUS='NEW')

```



```

OPEN(UNIT=5,FILE='BETA.MAT',STATUS='NEW')
OPEN(UNIT=6,FILE='GAMMA.MAT',STATUS='NEW')
C *****
C ENTER NO. OF INPUT,MIDDLE AND OUTPUT LAYER NEURONS
READ(1,*)INNO
READ(1,*)MIDNO
READ(1,*)NOUTNO
C ENTER NO. OF INPUT TRAINING DATAS
READ(1,*)NODATA
C ENTER NO. OF ITERATIONS
READ(1,*)ITER
C ENTER THE LEARNING RATE
READ(1,*)ETA
C *****
C READ THE TRAINING INPUT VALUES & THEIR CORRESPONDING
C OUTPUT VALUES
C *****
DO 10 I = 1,NODATA
READ(2,*)TDOT1(I),TDOT2(I),TDOT3(I)
READ(3,*)XDOT(I),YDOT(I),ZDOT(I)
FTDOT1(I) = (1.0D0/(1.0D0 + DEXP(-TDOT1(I))))
FTDOT2(I) = (1.0D0/(1.0D0 + DEXP(-TDOT2(I))))
FTDOT3(I) = (1.0D0/(1.0D0 + DEXP(-TDOT3(I))))
10 CONTINUE
C *****
C RANDOM NUMBER GENERATION FOR INITIAL INPUT AND
C OUTPUT WEIGHT MATRICES
C *****
C SEED FOR RANDOM NUMBER GENERATOR
ISEED = 23148
JSEED = 32124
DO 20 I = 1,MIDNO
DO 20 J = 1,INNO
RV = RAN(ISEED)*2.0D0 - 1.0D0
V(I,J) = RV
20 CONTINUE
DO 30 I = 1,NOUTNO
DO 30 J = 1,MIDNO
RW = RAN(JSEED)*2.0D0 - 1.0D0
30 CONTINUE
C *****
C TRAINING STARTS HERE
C *****
DO 40 NO = 1,ITER

```

```

C *****
DO 50 KD = 1,NODATA
RI(1) = XDOT(KD)
RI(2) = YDOT(KD)
RI(3) = ZDOT(KD)
DO 60 KR = 1,MIDNO
RM(KR) = 0.0D0
DO 70 KP = 1,INNO
RM(KR) = RM(KR) + V(KR,KP)*RI(KP)
70 CONTINUE
FRM(KR) = (1.0D0/(1.0D0 + DEXP(-RM(KR))))
FRMD(KR) = FRM(KR)*(1.0D0 - FRM(KR))
60 CONTINUE
DO 80 KR = 1,NOUTNO
RO(KR) = 0.0D0
DO 90 KP = 1,MIDNO
RO(KR) = RO(KR) + W(KR,KP)*FRM(KP)
90 CONTINUE
FRO(KR) = (1.0D0/(1.0D0 + DEXP(-RO(KR))))
FROD(KR) = FRO(KR)*(1.0D0 - FRO(KR))
80 CONTINUE
C *****
C ERROR UPDATE
C *****
DO 100 J = 1,MIDNO
EMS(J) = 0.0D0
100 CONTINUE
EOS(1) = FTDOT1(KD) - FRO(1)
EOS(2) = FTDOT2(KD) - FRO(2)
EOS(3) = FTDOT3(KD) - FRO(3)
DO 110 IE = 1,NOUTNO
DO 120 JE = 1,MIDNO
EMS(JE) = EMS(JE) + EOS(IE)*FROD(IE)*W(IE,JE)
120 CONTINUE
110 CONTINUE
C *****
C WEIGHT UPDATE
C *****
DO 200 IRT = 1,NOUTNO
DO 210 JRT = 1,MIDNO
W(IRT,JRT) = W(IRT,JRT) + ETA*EOS(IRT)*FROD(IRT)*FRM(JRT)
210 CONTINUE
200 CONTINUE
DO 220 IRT = 1,MIDNO

```

```

DO 230 JRT = 1,INNO
V(IRT,JRT) = V(IRT,JRT) + ETA*EMS(IRT)*FRMD(IRT)*RI(JRT)
230 CONTINUE
220 CONTINUE
C *****
DO 300 I = 1,MIDNO
RM(I) = 0.0D0
DO 310 J = 1,INNO
RM(I) = RM(I) + V(I,J)*RI(J)
310 CONTINUE
FRM(I) = (1.0D0 /(1.0D0 + DEXP(-RM(I))))
300 CONTINUE
DO 320 I = 1,NOUTNO
RO(I) = 0.0D0
DO 330 J = 1,MIDNO
RO(I) = RO(I) + W(I,J)*FRM(J)
330 CONTINUE
320 CONTINUE
C *****
C FINAL OUTPUT AT THE END OF EACH ITERATION
C *****
DTDOT1(KD) = RO(1)
DTDOT2(KD) = RO(2)
DTDOT3(KD) = RO(3)
50 CONTINUE
40 CONTINUE
C *****
C COMPARISON OF NEURAL AND ACTUAL OUTPUT
C *****
DO 500 IT = 1,NODATA
WRITE(4,*)DTDOT1(IT),TDOT1(IT)
WRITE(5,*)DTDOT2(IT),TDOT2(IT)
WRITE(6,*)DTDOT3(IT),TDOT3(IT)
500 CONTINUE
STOP
END

```

```

IMPLICIT REAL*8(A-H,O-Z)
DIMENSION TDOT1(100),TDOT2(100),TDOT3(100)
DIMENSION DTDOT1(100),DTDOT2(100),DTDOT3(100)
OPEN(UNIT=1,FILE='TDOT.MAT',STATUS='OLD')
OPEN(UNIT=3,FILE='ALPHA.MAT',STATUS='OLD')
OPEN(UNIT=4,FILE='BETA.MAT',STATUS='OLD')

```

```

OPEN(UNIT=5,FILE='GAMMA.MAT',STATUS='OLD')
OPEN(UNIT=6,FILE='REBAK.MAT',STATUS='NEW')
OPEN(UNIT=7,FILE='RERR.MAT',STATUS='NEW')
READ(*,*)NO
DO 10 I = 1, NO
  READ(1,*)TDDOT1(I),TDDOT2(I),TDDOT3(I)
  READ(3,*)DTDDOT1(I)
  READ(4,*)DTDDOT2(I)
  READ(5,*)DTDDOT3(I)
10  CONTINUE
  CALL MINMAX(TDDOT2,SMALL2,PLARGE2,NO)
  CALL MINMAX(TDDOT3,SMALL3,PLARGE3,NO)
  DO 20 I = 1,NO
    SDDOT2 = DTDDOT2(I)*(PLARGE2 - SMALL2) + SMALL2
    SDDOT3 = DTDDOT3(I)*(PLARGE3 - SMALL3) + SMALL3
    WRITE(6,*)SDDOT1,SDDOT2,SDDOT3
  C  TO FIND OUT THE MAGNITUDE OF ERROR
    UPP = TDDOT1(I) - SDDOT1
    VPP = TDDOT2(I) - SDDOT2
    WPP = TDDOT3(I) - SDDOT3
    ERR = SQRT(UPP*UPP + VPP*VPP + WPP*WPP)
    WRITE(7,*)ERR
  20  CONTINUE
    STOP
    END

C  *****
C  A SIMPLE PROGRAM FOR CHECKING THE CARTESIAN VELOCITIES
C  FOR A PUMA-560 MANIPULATOR
C  *****
IMPLICIT REAL*8(A-H,O-Z)
INTRINSIC DATAN2D,DSIND,DCOSD
DIMENSION RJ(3,3),VEL(3),THDT(3),RJINV(3,3)
DIMENSION FTHDT(3),TDDOT(3),OVEL(3),OTDDOT(3)
OPEN(UNIT=1,FILE='PUMA.DAT',STATUS='OLD')
OPEN(UNIT=2,FILE='RANG.MAT',STATUS='OLD')
OPEN(UNIT=7,FILE='REBAK.MAT',STATUS='OLD')
OPEN(UNIT=8,FILE='VDOT.MAT',STATUS='NEW')
OPEN(UNIT=9,FILE='TDDOT.MAT',STATUS='OLD')
OPEN(UNIT=10,FILE='OVDOT.MAT',STATUS='NEW')
READ(1,*)A2,A3,D3,D4
WRITE(*,*)'NO OF DATAS ?'
READ(*,*)NO
DO 43 I = 1,NO

```

```

READ(2,*)T1,T2,T3
S1 = DSIND(T1)
S2 = DSIND(T2)
C1 = DCOSD(T1)
C2 = DCOSD(T2)
C23 = DCOSD(T2+T3)
S23 = DSIND(T2+T3)
RJ(1,1) = -A3*S1*C23 + D4*S1*S23 - A2*C2*S1 - D3*C1
RJ(1,2) = -A3*C1*S23 - D4*C1*C23 - A2*S2*C1
RJ(1,3) = -A3*C1*S23 - D4*C1*C23
RJ(2,1) = A3*C1*C23 - D4*C1*S23 + A2*C2*C1 - D3*S1
RJ(2,2) = -A3*S1*S23 - D4*S1*C23 - A2*S2*S1
RJ(2,3) = -A3*S1*S23 - D4*S1*C23
RJ(3,1) = 0.0D0
RJ(3,2) = -A3*C23 + D4*S23 - A2*C2
RJ(3,3) = -A3*C23 + D4*S23
READ(7,*)TDOT(1),TDOT(2),TDOT(3)
READ(9,*)OTDOT(1),OTDOT(2),OTDOT(3)
CALL DMURRV(3,3,RJ,3,3,TDOT,1,3,VEL)
CALL DMURRV(3,3,RJ,3,3,OTDOT,1,3,OVEL)
WRITE(8,*)VEL(1),VEL(2),VEL(3)
WRITE(10,*)OVEL(1),OVEL(2),OVEL(3)
SS = SQRT(VEL(1)*VEL(1)+VEL(2)*VEL(2)+VEL(3)*VEL(3))
PS = SQRT(OVEL(1)*OVEL(1)+OVEL(2)*OVEL(2)+OVEL(3)*OVEL(3))
PRINT *,SS,PS
DO 50 INK = 1,3
DO 50 JNK = 1,3
RJ(INK,JNK) = 0.0D0
50 CONTINUE
43 CONTINUE
STOP
END

```

A.2 ACCELERATION ANALYSIS OF A TWO-LINK MANIPULATOR

```

C *****
C ACCELERATION ANALYSIS OF A TWO-LINK
C PLANAR MANIPULATOR
C
C STEPS FOLLOWED :
C *****
C
C 1. FIND OUT THE CO-ORDINATES OF THE CIRCULAR

```

```

C      PATH
C      2. FOR THE GIVEN COORDINATES FIND OUT THE JOINT
C      VARIABLES TH_K1 AND TH_K2
C      3. RESOLVE TANGENTIAL VELOCITY V_T IN THE GLOBAL
C      COORDINATE SYSTEM
C      4. EVALUATE THE ROTATION RATES THDT_K1 AND THDT_K2
C      USING JACOBIAN MATRIX
C      5. RESOLVE ACCELERATION A_P IN THE GLOBAL C.S
C      6. FIND OUT THE JOINT ACCELERATIONS THDDT_K1 AND
C      THDDT_K2
C      *****
c      STEP 1: FIND THE COORDINATES OF THE CIRCULAR
C      TRAJECTORY
c      *****
      IMPLICIT REAL*8(A-H,O-Z)
      INTRINSIC DSIND,DCOSD,DATAN2D
      REAL*8 TR1(4,4),TR2(4,4),TR3(4,4),XY(4),PV(4),TR4(4,4)
      REAL*8 TR5(4,4)
      OPEN(1, FILE = 'LINK.DET', STATUS = 'OLD')
      OPEN(2, FILE = 'XY.MAT', STATUS = 'NEW')
      READ(1,*)RL1,RL2
      READ(1,*)ST
      READ(1,*)NPOINT
C      STEP ANGLE FOR COORDINATE GENERATION
      READ(1,*)STANG
C      RADIUS
      READ(1,*)RD
      CALL TRANS(45.0,0.0,0.0,0.0,TR1)
      CALL TRANS(0.0,RL1,0.0,0.0,TR2)
      CALL MATMAT(TR1,TR2,TR3,4,4,4)
      PHI = ST
      DO 100 I = 1,NPOINT
      CALL TRANS(PHI,0.1,0.0,0.0,TR4)
      CALL MATMAT(TR3,TR4,TR5,4,4,4)
      PV(1) = RD
      PV(2) = 0.0D0
      PV(3) = 0.0D0
      PV(4) = 1.0D0
      CALL MATVEC(TR5,PV,XY,4,4)
      WRITE(2,*)XY(1),XY(2)
      PHI = PHI + STANG
100  CONTINUE
      STOP
      END

```

```

SUBROUTINE MATVEC(A,B,C,M,N)
IMPLICIT REAL*8(A-H,O-Z)
REAL*8 A(4,4),B(4),C(4)
DO 1200 I = 1,M
C(I) = 0.0D0
DO 1200 J = 1,N
C(I) = C(I) + A(I,J)*B(J)
1200 CONTINUE
RETURN
END

```

```

SUBROUTINE MATMAT(A,B,C,M,N,L)
IMPLICIT REAL*8(A-H,O-Z)
REAL*8 A(4,4),B(4,4),C(4,4)
DO 1300 I = 1,M
DO 1300 J = 1,N
C(I,J) = 0.0D0
DO 1300 K = 1,L
C(I,J) = C(I,J) + A(I,K)*B(K,J)
1300 CONTINUE
RETURN
END

```

```

SUBROUTINE ROTZ(ANG,RZ)
IMPLICIT REAL*8(A-H,O-Z)
INTRINSIC DSIND,DCOSD,DATAN2D
REAL*8 RZ(3,3)
RZ(1,1) = DCOSD(ANG)
RZ(1,2) = -DSIND(ANG)
RZ(1,3) = 0.0D0
RZ(2,1) = DSIND(ANG)
RZ(2,2) = DCOSD(ANG)
RZ(2,3) = 0.0D0
RZ(3,1) = 0.0D0
RZ(3,2) = 0.0D0
RZ(3,3) = 1.0D0
RETURN
END

```

```

SUBROUTINE TRANS(ANG,PX,PY,PZ,TR)
IMPLICIT REAL*8(A-H,O-Z)
INTRINSIC DSIND,DCOSD,DATAN2D
REAL*8 TR(4,4)

```

```

TR(1,1) = DCOSD(ANG)
TR(1,2) = -DSIND(ANG)
TR(1,3) = 0.0D0
TR(1,4) = PX
TR(2,1) = DSIND(ANG)
TR(2,2) = DCOSD(ANG)
TR(2,3) = 0.0D0
TR(2,4) = PY
TR(3,1) = 0.0D0
TR(3,2) = 0.0D0
TR(3,3) = 1.0D0
TR(3,4) = 0.0D0
TR(4,1) = 0.0D0
TR(4,2) = 0.0D0
TR(4,3) = 0.0D0
TR(4,4) = 1.0D0
RETURN
END

```

```

C *****
C STEP 2: FIND THE JOINT COORDINATES FOR THE
C CIRCULAR TRAJECTORY
C *****
IMPLICIT REAL*8(A-H,O-Z)
INTRINSIC DSIND,DCOSD,DATAN2D,DSQRT
REAL*8 THET(4)
OPEN(1, FILE = 'LINK.DET', STATUS = 'OLD')
OPEN(2, FILE = 'XY.MAT', STATUS = 'OLD')
OPEN(3, FILE = 'THET.MAT', STATUS = 'NEW')
READ(1,*)RL1,RL2
READ(1,*)ST
READ(1,*)NPOINT
C STEP ANGLE FOR COORDINATE GENERATION
READ(1,*)STANG
DO 200 I = 1,NPOINT
READ(2,*)XP,YP
RJ = 2.0D0 * YP * RL1
RII = 2.0D0 * XP * RL1
RKK = XP*XP + YP*YP + RL1*RL1 - RL2*RL2
RTT = RJ*RJ + RII*RII - RKK*RKK
THET(1) = DATAN2D(RJ,RII) + DATAN2D(DSQRT(RTT),RKK)
PAR1 = YP - RL1*DSIND(THET(1))
PAR2 = XP - RL1*DCOSD(THET(1))
THET(2) = DATAN2D(PAR1,PAR2) - THET(1)

```



```

WRITE(3,*)THET(1),THET(2)
200 CONTINUE
STOP
END

C *****
C STEP 3: RESOLVE TANGENTIAL VELOCITY V_T IN THE
c GLOBAL COORDINATE SYSTEM
C *****
IMPLICIT REAL*8(A-H,O-Z)
INTRINSIC DSIND,DCOSD,DATAN2D
REAL*8 XY(2),VP(3),RZZA(3,3),VPG(3)
OPEN(1, FILE = 'LINK.DET', STATUS = 'OLD')
OPEN(2, FILE = 'VTRES.DAT', STATUS = 'OLD')
OPEN(3, FILE = 'XY.MAT', STATUS = 'OLD')
OPEN(4, FILE = 'VPG.MAT', STATUS = 'NEW')
READ(1,*)RL1,RL2
READ(1,*)ST
READ(1,*)NPOINT
C STEP ANGLE FOR COORDINATE GENERATION
READ(1,*)STANG
READ(2,*)V_T,XC,YC,RAD
DO 300 I = 1,NPOINT
READ(3,*)XY(1),XY(2)
PKL = XY(2)-YC
PKK = XY(1)-XC
ALPH = DATAN2D(PKL,PKK)
VP(1) = V_T*DCOSD(90.0D0+ALPH)
VP(2) = V_T*DCOSD(ALPH)
VP(3) = 1.0D0
WRITE(4,*)VP(1),VP(2)
300 CONTINUE
STOP
END

C *****
C STEP 4: EVALUATE THE ROTATION RATES THDT_K1 AND THDT_K2
C USING JACOBIAN MATRIX
C *****
IMPLICIT REAL*8(A-H,O-Z)
INTRINSIC DSIND,DCOSD,DATAN2D
REAL*8 THET(2),VPG(2),THDT(2),RINV(2,2)

```

```

OPEN(1, FILE = 'LINK.DET', STATUS = 'OLD')
OPEN(2, FILE = 'THET.MAT', STATUS = 'OLD')
OPEN(3, FILE = 'VPG.MAT', STATUS = 'OLD')
OPEN(4, FILE = 'THDT.MAT', STATUS = 'NEW')
READ(1,*)RL1,RL2
READ(1,*)ST
READ(1,*)NPOINT
C STEP ANGLE FOR COORDINATE GENERATION
READ(1,*)STANG
DO 400 I = 1,NPOINT
READ(2,*)THET(1),THET(2)
READ(3,*)VPG(1),VPG(2)
UT11 = -RL1*DSIND(THET(1)) - RL2*DSIND(THET(1)+THET(2))
UT12 = -RL2*DSIND(THET(1)+THET(2))
UT21 = RL1*DCOSD(THET(1)) + RL2*DCOSD(THET(1)+THET(2))
UT22 = RL2*DCOSD(THET(1)+THET(2))
DET = UT11*UT22 - UT21*UT12
RINV(1,1) = UT22/DET
RINV(1,2) = -UT12/DET
RINV(2,1) = -UT21/DET
RINV(2,2) = UT11/DET
CALL MATVEC(RINV,VPG,THDT,2,2)
WRITE(4,*)THDT(1),THDT(2)
400 CONTINUE
STOP
END

C *****
C STEP 5: RESOLVE ACCELERATION A_P IN THE GLOBAL
C COORDINATE SYSTEM
C *****
IMPLICIT REAL*8(A-H,O-Z)
INTRINSIC DSIND,DCOSD,DATAN2D
REAL*8 XY(2),AP(3),RZAP(3,3),APG(3),bp(2)
OPEN(1, FILE = 'LINK.DET', STATUS = 'OLD')
OPEN(2, FILE = 'VTRES.DAT', STATUS = 'OLD')
OPEN(3, FILE = 'XY.MAT', STATUS = 'OLD')
OPEN(4, FILE = 'APG.MAT', STATUS = 'NEW')
READ(1,*)RL1,RL2
READ(1,*)ST
READ(1,*)NPOINT
C STEP ANGLE FOR COORDINATE GENERATION
READ(1,*)STANG
READ(2,*)V_T,XC,YC,RAD

```

```

DO 300 I = 1,NPOINT
  READ(3,*)XY(1),XY(2)
  PKK = XY(2)-YC
  PKL = XY(1)-XC
  ALPH = DATAN2D(PKK,PKL)
  AP(1) =  $(-V\_T \cdot V\_T / \text{RAD}) \cdot \text{DCOSD}(\text{ALPH})$ 
  AP(2) =  $(-V\_T \cdot V\_T / \text{RAD}) \cdot \text{DSIND}(\text{ALPH})$ 
  AP(3) = 1.0D0
  WRITE(4,*) AP(1),AP(2)
300 CONTINUE
STOP
END

C *****
C STEP 6: FIND OUT THE JOINT ACCELERATIONS THDDT_K1 AND
C THDDT_K2
C *****
IMPLICIT REAL*8(A-H,O-Z)
INTRINSIC DSIND,DCOSD,DATAN2D
REAL*8 THET(2),VPG(2),THDT(2),RINV(2,2),THDDT(2)
REAL*8 APG(2),AXT(2),PXT(2),PT1(2,2)
OPEN(1, FILE = 'LINK.DET', STATUS = 'OLD')
OPEN(2, FILE = 'THET.MAT', STATUS = 'OLD')
OPEN(3, FILE = 'VPG.MAT', STATUS = 'OLD')
OPEN(4, FILE = 'THDT.MAT', STATUS = 'OLD')
OPEN(7, FILE = 'APG.MAT', STATUS = 'OLD')
OPEN(8, FILE = 'THDDT.MAT', STATUS = 'NEW')
READ(1,*)RL1,RL2
READ(1,*)ST
READ(1,*)NPOINT
C STEP ANGLE FOR COORDINATE GENERATION
READ(1,*)STANG
DO 400 I = 1,NPOINT
  READ(2,*)THET(1),THET(2)
  READ(3,*)VPG(1),VPG(2)
  READ(4,*)THDT(1),THDT(2)
  READ(7,*)APG(1),APG(2)
  PT1(1,1) =  $-RL1 \cdot \text{DCOSD}(\text{THET}(1)) \cdot \text{THDT}(1)$ 
% -  $RL2 \cdot \text{DCOSD}(\text{THET}(1) + \text{THET}(2)) \cdot (\text{THDT}(1) + \text{THDT}(2))$ 
  PT1(1,2) =  $-RL2 \cdot \text{DCOSD}(\text{THET}(1) + \text{THET}(2)) \cdot (\text{THDT}(1) + \text{THDT}(2))$ 
  PT1(2,1) =  $-RL1 \cdot \text{DSIND}(\text{THET}(1)) \cdot \text{THDT}(1)$ 
% -  $RL2 \cdot \text{DSIND}(\text{THET}(1) + \text{THET}(2)) \cdot (\text{THDT}(1) + \text{THDT}(2))$ 
  PT1(2,2) =  $-RL2 \cdot \text{DSIND}(\text{THET}(1) + \text{THET}(2)) \cdot (\text{THDT}(1) + \text{THDT}(2))$ 

```

```

CALL MATVEC(PT1,THDT,AXT,2,2)
PXT(1) = APG(1) - AXT(1)
PXT(2) = APG(2) - AXT(2)
UT11 = -RL1*DSIND(THET(1)) - RL2*DSIND(THET(1)+THET(2))
UT12 = -RL2*DSIND(THET(1)+THET(2))
UT21 = RL1*DCOSD(THET(1)) + RL2*DCOSD(THET(1)+THET(2))
UT22 = RL2*DCOSD(THET(1)+THET(2))
DET = UT11*UT22 - UT21*UT12
RINV(1,1) = UT22/DET
RINV(1,2) = -UT12/DET
RINV(2,1) = -UT21/DET
RINV(2,2) = UT11/DET
CALL MATVEC(RINV,PXT,THDDT,2,2)
WRITE(8,*)THDDT(1),THDDT(2)
400 CONTINUE
STOP
END

C *****
C GENERATION OF [C] MATRIX FOR LINEAR PROGRAMMING
C *****
DIMENSION X1(23),X2(23),X3(23),X4(23),X5(23)
DIMENSION X6(23),X7(23),X8(23),X9(23),X10(23)
DIMENSION A(1,1100),Y(23)
OPEN(1, FILE = 'ALPGa.IN', STATUS = 'OLD')
OPEN(2, FILE = 'CLPGa.OUT', STATUS = 'NEW')
DO 14 I = 1,23
  READ(1,*)X1(I)
14 CONTINUE
DO 15 I = 1,23
  READ(1,*)X2(I)
15 CONTINUE
DO 16 I = 1,23
  READ(1,*)X3(I)
16 CONTINUE
DO 17 I = 1,23
  READ(1,*)X4(I)
17 CONTINUE
DO 18 I = 1,23
  READ(1,*)X5(I)
18 CONTINUE
DO 19 I = 1,23
  READ(1,*)X6(I)
19 CONTINUE

```

```

DO 20 I = 1,23
  READ(1,*)X7(I)
20  CONTINUE
  DO 21 I = 1,23
    READ(1,*)X8(I)
21  CONTINUE
    DO 22 I = 1,23
      READ(1,*)X9(I)
22  CONTINUE
      DO 23 I = 1,23
        READ(1,*)X10(I)
23  CONTINUE
        DO 44 K = 1,23
          Y(K) = X1(K) + X2(K) + X3(K) + X4(K) + X5(K) + X6(K) + X7(K)
          # + X8(K) + X9(K) + X10(K)
44  CONTINUE
          NS = 1
          NT = 46
80  CONTINUE
          IF(NT.GT.1100) GOTO 100
          MT = 1
          DO 310 I = NS,NT,2
            A(1,I) = Y(MT)
            MT = MT + 1
310 CONTINUE
            MT = 1
            DO 320 I = NS+1,NT,2
              A(1,I) = -Y(MT)
              MT = MT + 1
320 CONTINUE
              DO 330 I = NT+1,NT+4
                A(1,I) = 10.0
330 CONTINUE
                DO 340 I = NT+2,NT+3
                  A(1,I) = -10.0
340 CONTINUE
                  NS = NS + 50
                  NT = NT + 50
                  GO TO 80
100 CONTINUE
1050 CONTINUE
      WRITE(2,*)(A(1,J),J = 1,1100)
      STOP
      END

```

```

C *****LPNEURO.FOR*****
C LP-NEURO METHOD SUBROUTINE
C *****
C A LP APPROACH FOR NEURAL NETWORKS
C *****
  DIMENSION YX(1),YXSTRT(1),RMAX(1),RMIN(1),PHI(1),PSI(1)
  DIMENSION YW(150),ZX(1100),ZA(220,1100),ZB(220),ZC(1100)
  DIMENSION ZAP(220,1100),ZCP(1100),ZBP(220),ZW(50000)
  DIMENSION BBW(22,23),BBC(22),BBD(22),ZTOB(23)
  COMMON
% /SEEK/IDATA,IPRINT,NSHOT,NTEST,MAXM,F,G,TOL,ZERO,
% R,REDUCE
  COMMON /BL1/ZC,ZX,ZW,ZAP,ZCP,ZBP
  COMMON /BL3/ZB
  COMMON /BL2/MZ,NZ,NUTS,NT,NI,NOUT,NOI
  COMMON /FAL/ZTOB
  COMMON /ANT/ZA
  OPEN(2, FILE = 'BLPGA.OUT', STATUS = 'OLD')
  OPEN(3, FILE = 'CLPGA.OUT', STATUS = 'OLD')
  OPEN(14, FILE = 'LIN.DAT', STATUS = 'OLD')
  OPEN(15, FILE = 'KARI.DAT', STATUS = 'OLD')
  OPEN(8, FILE = 'OBJ.MAT', STATUS = 'NEW')
  OPEN(10, FILE = 'FWT.MAT', STATUS = 'NEW')
  READ(14,*)MZ
  READ(14,*)NZ
  READ(14,*)NUTS
  READ(14,*)NT,NI
  READ(14,*)NOUT,NOI
  DO 884 I = 1,23
  READ(15,*)ZTOB(I)
884  CONTINUE
  MAXM = 10
  CALL ALPG
  DO 196 I = 1,MZ
  READ(2,*)ZB(I)
196  CONTINUE
  READ(3,*)(ZC(I),I = 1,NZ)
  NY = 1
  NCONS = 0
  NEQUS = 0
  NPENAL = 3
  IDATA = 0
  DATA RMAX/10.0/

```

```

DATA RMIN/-10.0/
DATA YXSTRT/0.611/
NOISE = 1
CALL
SEEK(NY,NCONS,NEQUS,NPENAL,RMAX,RMIN,YXSTRT,YX,YU,PHI,
% PSI,NVIOL,YW)
CALL ANSWER(YU,YX,PHI,PSI,NY,NCONS,NEQUS)
WRITE(*,*)'DO YOU WISH TO CONTINUE ?'
WRITE(*,*)'1: YES '
WRITE(*,*)'2: NO '
READ(*,*)NDEC
IF(NDEC.EQ.1) THEN
GO TO 1
ELSE
END IF
STOP
END

```

```

SUBROUTINE UREAL(YX,YU)
DIMENSION YX(1),YXSTRT(1),RMAX(1),RMIN(1),PHI(1),PSI(1)
DIMENSION YW(150),ZX(1100),ZA(220,1100),ZB(220),ZC(1100)
DIMENSION ZAP(220,1100),ZBP(220),ZCP(1100)
DIMENSION ZW(50000),ZTOB(22)
DIMENSION BBW(22,23),BBC(22),BBD(22),D(2)
DIMENSION SAK(4),RT3(22)
COMMON /BL1/ZC,ZX,ZW,ZAP,ZCP,ZBP
COMMON /BL3/ZB
COMMON /BL2/MZ,NZ,NUTS,NT,NI,NOUT,NOI
COMMON /SIMPLE/NSTOP,IDATA,NNDEX
COMMON /PAKS/BBW,BBC,BBD
COMMON /FAL/ZTOB
COMMON /ANT/ZA
COMMON /DEPUT/D,RMX,RMN
IDATA = 0
NNDEX = 3
DO 20 I = 1,MZ
KR = 1
DO 30 J = 1,NZ
IF(J.GT.(50*KR)) THEN
KR = KR + 1
END IF
IF((J.GE.(1+50*(KR-1))).AND.(J.LT.(47+50*(KR-1)))) THEN
ZAP(I,J) = YX(1)*ZA(I,J)

```

```

ELSE
ZAP(I,J) = ZA(I,J)
END IF
30  CONTINUE
20  CONTINUE
SQM = 0.0
DO 40 I = 1,MZ
ZBP(I) = YX(1)*ZB(I)
SQM = SQM + ZB(I)
40  CONTINUE
KR = 1
DO 50 J = 1,NZ
IF(J.GT.(50*KR)) THEN
KR = KR + 1
END IF
IF((J.GE.(1 + 50*(KR-1))).AND.(J.LT.(47+50*(KR-1)))) THEN
ZCP(J) = YX(1)*ZC(J)
ELSE
ZCP(J) = ZC(J)
END IF
50  CONTINUE
CALL SIMPLE(NZ,MZ,ZAP,ZBP,ZCP,ZX,ZU,ZW)
CALL WASS(ZX,BBW,BBC,BBD)
YT1 = 0.0
YT2 = 0.0
YT3 = 0.0
DO 55 NM = 1,46,2
DO 60 MM = NM,1100,50
PRINT *,YX(1),ZC(NM),ZX(MM)
YT1 = YX(1)*(ZC(NM)*ZX(MM)) + YT1
60  CONTINUE
55  CONTINUE
DO 65 NM = 2,46,2
DO 70 MM = NM,1100,50
YT2 = YX(1)*(ZC(NM)*ZX(MM)) + YT2
70  CONTINUE
65  CONTINUE
DO 75 NM = 47,50
DO 80 MM = NM,1100,50
YT3 = (ZC(NM)*ZX(MM)) + YT3
80  CONTINUE
75  CONTINUE
YT4 = YX(1)*SQM
CALL RMIXD(BBW,BBC,BBD,YX,ZTOB,RT3)

```



```

YU = (YT1 + YT2 + YT3 - YT4)**2
WRITE(*,*)'SLOPE IS',YX(1)
WRITE(*,*)'SEEK OBJECTIVE FUNCTION IS',YU
IF (NSW.EQ.1) THEN
STOP
END IF
IF(YU.LT.(2.0E-4)) THEN
CALL RMIXD(BBW,BBC,BBD,YX,ZTOB,RT3)
WRITE(18,*)'LAST ITERATION'
WRITE(18,*)(RT3(JK),JK=1,22)
NSW = 1
ELSE
END IF
RETURN
END

```

```

SUBROUTINE CONST(YX,NCONS,PHI)
DIMENSION PHI(1),D(2),YX(1)
COMMON /DEPUT/D,RMX,RMN
PRINT *, 'SEEK ITERATIONS',NOISE
NOISE = NOISE + 1
RETURN
END

```

```

SUBROUTINE EQUAL(YX,PSI,NEQUS)
DIMENSION YX(1),PSI(1)
RETURN
END

```

```

SUBROUTINE W^SS(ZX,BBW,BBC,BBD)
DIMENSION ZX(1100),BBW(22,23),BBC(22),BBD(22)
ND = 1
RAMYA = 0.0
DO 432 I = 1,22
DO 433 J = 1,23
RAMYA = ZX(ND) - ZX(ND + 1)
BBW(I,J) = RAMYA
ND = ND + 2
433 CONTINUE
BBC(I) = ZX(ND) - ZX(ND + 1)
ND = ND + 2
BBD(I) = ZX(ND) - ZX(ND + 1)
ND = ND + 2

```

```

432  CONTINUE
      RETURN
      END

      SUBROUTINE RMIXD(PBW,BBC,BBD,YX,ZTOB,RT3)
      DIMENSION YX(1),CBC(22),CBD(22),RT1(22),RT2(22),RT3(22)
      DIMENSION ZTOB(23),BBW(22,23),BBC(22),BBD(22)
      DO 2339 I = 1,22
      CBC(I) = 0.0
      CBD(I) = 0.0
      RT1(I) = 0.0
      RT2(I) = 0.0
      RT3(I) = 0.0
2339  CONTINUE
      CALL RMATMUL(BBW,ZTOB,RT1,22,23)
      DO 2340 I = 1,22
      CBC(I) = (1.0/YX(1))*BBC(I)
      CBD(I) = (1.0/YX(1))*BBD(I)
2340  CONTINUE
      CALL RMATADD(RT1,CBC,RT2,22)
      CALL RMATSUB(RT2,CBD,RT3,22)
      WRITE(18,*)(RT3(JK),JK=1,22)
      RETURN
      END

      SUBROUTINE RMATMUL(A,B,C,M,N)
      DIMENSION A(M,N),B(N),C(M)
      DO 4430 I = 1,M
      C(I) = 0.0
      DO 4440 J = 1,N
      C(I) = C(I) + A(I,J)*B(J)
4440  CONTINUE
4430  CONTINUE
      RETURN
      END

      SUBROUTINE RMATADD(A,B,C,M)
      DIMENSION A(M),B(M),C(M)
      DO 4256 I = 1,M
      C(I) = A(I) + B(I)
4256  CONTINUE
      RETURN
      END

```

```

SUBROUTINE RMATSUB(A,B,C,M)
  DIMENSION A(M),B(M),C(M)
  DO 4169 I = 1,M
    C(I) = A(I) - B(I)
4169  CONTINUE
  RETURN
END

SUBROUTINE ALPG
C  GENERATION OF [A] MATRIX FOR LINEAR PROGRAMMING
  DIMENSION X(23),ZA(220,1100)
  COMMON /ANT/ZA
  OPEN(17, FILE = 'ALPGA.IN', STATUS = 'OLD')
  DO 1050 NI = 1,220,22
    KNI = NI
    NS = 1
    NT = 46
    DO 714 I = 1,23
      READ(17,*)X(I)
714  CONTINUE
780  CONTINUE
    IF(NT.GT.1100) GOTO 7100
    MT = 1
    DO 710 I = NS,NT,2
      ZA(KNI,I) = X(MT)
      MT = MT + 1
710  CONTINUE
    MT = 1
    DO 720 I = NS+1,NT,2
      ZA(KNI,I) = -X(MT)
      MT = MT + 1
720  CONTINUE
    DO 730 I = NT+1,NT+4
      ZA(KNI,I) = 1.0
730  CONTINUE
    DO 740 I = NT+2,NT+3
      ZA(KNI,I) = -1.0
740  CONTINUE
    KNI = KNI + 1
    NS = NS + 50
    NT = NT + 50
    GO TO 780
7100 CONTINUE
1050 CONTINUE

```

RETURN
END

Backpropagation Method - Multilayer Neural Network
/**

PROGRAM DESCRIPTION:

THIS PROGRAM ALLOWS A USER TO BUILD A GENERALIZED DELTA RULE NET FOR SUPERVISED LEARNING. USER CAN SPECIFY THE NUMBER OF INPUT & OUTPUT UNITS, NUMBER OF HIDDEN LAYERS AND NUMBER OF UNITS IN EACH HIDDEN LAYER. AFTER THE NET IS BUILT, LEARNING TAKES PLACE IN THE NET WITH A GIVEN SET OF TRAINING SAMPLES. USER SPECIFIES VALUES OF THE LEARNING RATE ETA, THE MOMENTUM RATE ALPHA, MAXIMUM TOLERANCE ERRORS AND MAXIMUM NUMBER OF ITERATIONS.

AFTER LEARNING, ALL THE INFORMATION RELEVANT TO THE STRUCTURE OF THE NET, INCLUDING WEIGHTS AND THRESHOLDS ARE STORED IN FILES.

OUTPUTS CAN BE GENERATED FOR NEW PATTERNS BY READING FROM FILE AND BY RECONSTRUCTING THE NET.

TRAINING SET SAMPLES AND ADDITIONAL SAMPLES FOR PROCESSING ARE STORED IN FILES.

*/

```
#include <stdio.h>
#include <math.h>
#include <ctype.h>
#include <curses.h>
#ifdef VAX /* for declaration of calloc() on PC or compatible */
#include <malloc.h>
#endif

/* define constants used throughout functions */

#define NMXUNIT 50 /* max no. of units in a layer (50) */
#define NMXHLLR 5 /* max no. of hidden layers (5) */
#define NMXOATTR 50 /* max no. of output features (50) */
#define NMXINP 200 /* max no. of input samples (200) */
```

```

#define NMXIATTR 50 /* max no. of input features (50) */
#define SEXIT 3 /* exit successfully */
#define RESTRT 2 /* restart */
#define FEXIT 1 /* exit in failure */
#define CONTNE 0 /* continue calculation */

```

```

/* Data base : declarations of variables */

```

```

float eta; /* learning rate */
float alpha; /* momentum rate */
float err_curr; /* normalized system error */
float maxe; /* max allowed system error */
float maxep; /* max allowed patter error */
float *wtptr[NMXHLR+1];
float *outptr[NMXHLR+2];
float *errptr[NMXHLR+2];
float *delw[NMXHLR+1];
float target[NMXINP][NMXOATTR];
float input[NMXINP][NMXIATTR], ep[NMXINP];
float outpt[NMXINP][NMXOATTR];
int nunit[NMXHLR+2], nhlayer, ninput, ninattr, noutattr;
int result, cnt, cnt_num;
int nsnew, nsold;
char task_name[20];
FILE *fp1, *fp2, *fp3, *fopen(), *foutt;
int fplot10;

```

```

/* random number generator
(computer independent) */

```

```

long randseed = 568731L;
int random()
{
    randseed = 15625L * randseed + 22221L;
    return((randseed >> 16) & 0x7FFF);
}

```

```

/* allocate dynamic storage for the set */

```

```

void init()
{
    int len1, len2, i, k;
    float *p1, *p2, *p3, *p4;

    len1 = len2 = 0;

```

```

nunit[nhlayer+2] = 0;

for (i=0; i<(nhlayer + 2); i++) {
    len1 += (nunit[i] + 1) * nunit[i+1];
    len2 += nunit[i] + 1;
}

/* weights */
p1=(float *) calloc(len1+1,sizeof(float));
/* output */
p2=(float *) calloc(len2+1,sizeof(float));
/* errors */
p3=(float *) calloc(len2+1,sizeof(float));
/* delw */
p4=(float *) calloc(len1+1,sizeof(float));

/* set up initial pointers */
wtptr[0] = p1;
outptr[0] = p2;
errptr[0] = p3;
delw[0] = p4;

/* set up the rest of pointers */
for (i=1; i < (nhlayer + 1); i++) {
    wtptr[i] = wtptr[i-1] + nunit[i] * (nunit[i-1] + 1);
    delw[i] = delw[i-1] + nunit[i] * (nunit[i-1] + 1);
}
for (i=1; i < (nhlayer + 2); i++) {
    outptr[i] = outptr[i-1] + nunit[i-1] + 1;
    errptr[i] = errptr[i-1] + nunit[i-1] + 1;
}

/* set up threshold outputs */
for (i=0; i < nhlayer + 1; i++) {
    *(outptr[i] + nunit[i]) = 1.0;
}
}

/* initialize weights with random
numbers between -1.0 and +1.0 */
void initwt()
{
    int i, j;

```

```

for (j=0; j < nhlayer + 1; j++)
    for (i=0; i < (nunit[j] + 1) * nunit[j + 1]; i++) {
        *(wptr[j] + i) = (random() / pow(2.0,15.0))*2.0 - 1.0;
        *(delw[j] + i) = 0.0;
    }
}

/* specify architecture of net and
values of learning parameters */
void set_up()
{
    int i;

    eta = 0.9;
    printf("\nMomentum rate eta (default = 0.9)? : ");
    scanf("%f", &eta);

    alpha = 0.7;
    printf("\nLearning rate alpha (default = 0.7)? : ");
    scanf("%f", &alpha);

    maxe = 0.01; maxep = 0.001;
    printf("\nMax total error (default = 0.01)? : ");
    scanf("%f", &maxe);
    printf("\nMax individual error (default = 0.001)? : ");
    scanf("%f", &maxep);

    cnt_num = 1000;
    printf("\nMax number of iterations (default = 1000)? : ");
    scanf("%d", &cnt_num);

    printf("\nNumber of hidden layers? : ");
    scanf("%d", &nhlayer);

    for (i=0; i < nhlayer; i++) {
        printf("\n\tNumber of units for hidden layer %d?: ", i+1);
        scanf("%d", &nunit[i+1]);
    }

    printf("\nCreate error file? (Enter 1 for yes, 0 for no) : ");
    scanf("%d", &fplot10);

    printf("\nExecution starts ");
    printf(" -- if many iterations specified, go out for coffee...\n");

```

```

    nunit[nhlayer+1] = noutattr;
    nunit[0] = ninattr;
}

/* read file for net architecture and learning
parameters. File name has suffix _v.dat */
void dread(char *taskname)
{
    int i,j,c;
    char var_file_name[20];

    strcpy(var_file_name, taskname);
    strcat(var_file_name, " v.dat");
    if ((fp1 = fopen(var_file_name, "r")) == NULL)
    {
        perror("\n Cannot open data file ");
        exit(0);
    }

    fscanf(fp1, "%d%d%d%f%f%d", &ninput, &noutattr, &ninattr,
        &eta, &alpha, &nhlayer, &cnt_num);
    for (j=0; j < nhlayer + 2; j++)
        fscanf(fp1, "%d", &nunit[j]);

    if ((c=fclose(fp1)) != 0)
        printf("\nFile %s cannot be closed; error %d ",
            var_file_name, c);
}

/* read file containing weights and thresholds
and thresholds. File name has suffix _w.dat */
void wread(char *taskname)
{
    int i,j,c;
    char wt_file_name[20];

    strcpy(wt_file_name, taskname);
    strcat(wt_file_name, " w.dat");
    if ((fp2 = fopen(wt_file_name, "r")) == NULL)
    {
        perror("\n Cannot open data file ");
        exit(0);
    }
}

```



```

    for (i=0; i < nhlayer + 1; i++) {
        for (j=0; j < (nunit[i] + 1) * nunit[i + 1]; j++) {
            fscanf(fp2, "%f", (wtptr[i]+j));
        }
    }

    if ((c = fclose(fp2)) != 0)
        printf("\n File %sf cannot be closed; error %d ",
            wt_file_name, c);

}

/* create file for net architecture and learning
parameters. File name has suffix _v.dat */

void dwrite(char *taskname)
{
    int i,j,c;
    char var_file_name[20];

    strcpy(var_file_name, taskname);
    strcat(var_file_name, "_v.dat");
    if ((fp1 = fopen(var_file_name, "w+")) == NULL)
    {
        perror(" Cannot open data file ");
        exit(0);
    }
    fprintf(fp1, "%u %u %u %f %f %u %u\n", ninput, noutattr,
        ninattr, eta, alpha, nhlayer, cnt_num);

    for (i=0; i < nhlayer + 2; i++) {
        fprintf(fp1, "%d ", nunit[i]);
    }

    fprintf(fp1, "\n%d %f\n", cnt, err_curr);

    for (i=0; i < ninput; i++)
    {
        for (j=0; j < noutattr; j++)
            fprintf(fp1, "%f ", outpt[i][j]);
        fprintf(fp1, "\n");
    }
}

```

```

        if ((c=fclose(fp1)) != 0)
            printf("\nFile %s cannot be closed; error %d ",
                var_file_name, c);
    }

    /* create file for saving weights and thresholds
       learned from training. File name has suffix
       _w.dat */

void wtwrite(char *taskname)
{
    int i,j,c,k;
    char wt_file_name[20];

    strcpy(wt_file_name, taskname);
    strcat(wt_file_name, "_w.dat");

    if ((fp2 = fopen(wt_file_name, "w+")) == NULL)
    {
        perror("\nCannot open data file ");
        exit(0);
    }

    k=0;
    for (i=0; i < nhlayer + 1; i++)
        for (j=0; j < (nunit[i] + 1) * nunit[i + 1]; j++) {
            if(k==8) {
                k=0;
                fprintf(fp2, "\n");
            }
            fprintf(fp2, "%f ", *(wtptr[i] + j));
            k++;
        }
    if ((c=fclose(fp2)) != 0)
        printf("\nFile %s cannot be closed; error %d ",
            wt_file_name, c);
}

/* bottom_up calculation of net for input
   pattern i */

void forward(int i)
{
    int m,n,p,offset;

```

```

float net;

/* input level output calculation */

for (m=0; m < ninattr; m++)
    *(outptr[0]+m) = input[i][m];

/* hidden & output layer output calculation */

for (m=1; m < nhlayer + 2; m++) {
    for (n=0; n < nunit[m]; n++) {
        net = 0.0;
        for (p=0; p < nunit[m-1] + 1; p++) {
            offset = (nunit[m-1] + 1) * n + p;
            net += *(wtptr[m-1] + offset) *
                (*(outptr[m-1] + p));
        }
        *(outptr[m]+n) = (2.0 / (1.0 + exp(-net)))-1.0;
    }
}
for (n=0; n < nunit[nhlayer + 1]; n++)
    outpt[i][n] = *(outptr[nhlayer + 1] + n);
}

/* several conditions are checked to see
whether learning should terminate */

int introspective(int nfrom, int nto)
{
    int i, flag;
    int kke;
    /* initscr();
    move(10,40);
    refresh();
    printf("%d",cnt); */
    /* reached max. iteration */
    if (cnt >= cnt_num) return(FEXIT);

    /* error for each pattern small enough? */
    nsnew = 0;
    flag = 1;
    for (i = nfrom; (i < nto) && (flag == 1); i++) {
        if (epf[i] <= maxep) nsnew++;
        else flag = 0;
    }
}

```

```

    }
    if (flag == 1) return (SEXIT);

    /* system total error small enough? */
    if (err_curr <= maxe) return (SEXIT);
    return(CONTNE);
}

/* threshold is treated as weight of link from
   a virtual node whose output value is unity */
int rumelhart(int from_snum, int to_snum)
{
    int i,j,k,m,n,p,offset,index;
    float out;
    char *err_file = "criter.dat";

    nsold = 0;
    cnt = 0;
    result = CONTNE;

    if (fplot10)
        if ((fp3 = fopen(err_file, "w")) == NULL)
        {
            perror( "\nCannot open error file ");
            exit(0);
        }
        do {
            err_curr = 0.0;
            /* for each pattern */
            for (i=from_snum; i < to_snum; i++) {
                forward(i); /* bottom_up calculation */

                /* top_down error propagation */
                /* output_level error */
                for (m=0; m < nunit[nhlayer + 1]; m++) {
                    out = *(outptr[nhlayer + 1] + m);
                    *(errptr[nhlayer + 1] + m) = (target[i][m] - out) *
                        0.5 * (1 - out*out);
                }

                /* hidden & input layer errors */
                for (m=nhlayer + 1; m >= 1; m--) {
                    for (n=0; n < nunit[m-1]+1; n++) {
                        *(errptr[m-1] + n) = 0.0;

```

```

    for (p=0; p < nunit[m]; p++) {
        offset = (nunit[m-1] + 1) * p + n;
        *(delw[m-1]+offset) = eta * (*(errptr[m]+p))
            * (*(outptr[m-1] + n))
            + alpha * (*(delw[m-1] + offset));
        *(errptr[m-1]+n) += *(errptr[m] + p)
            * (*(wtptr[m-1] + offset));
    }
    *(errptr[m-1] + n) = *(errptr[m-1] + n) *
        (1 - *(outptr[m-1] + n)
            * (*(outptr[m-1] + n)));
}

/* weight changes */
for (m=1; m < nhlayer + 2; m++) {
    for (n=0; n < nunit[m]; n++) {
        for (p=0; p < nunit[m-1] + 1; p++) {
            offset = (nunit[m-1] + 1) * n + p;
            *(wtptr[m-1] + offset) += *(delw[m-1] + offset);
        }
    }
}

ep[i] = 0.0;
for (m=0; m < nunit[nhlayer + 1]; m++) {
    ep[i] += fabs((target[i][m] -
        *(outptr[nhlayer+1] + m)));
}
err_curr += ep[i] * ep[i];
} /* no:malized system error */
err_curr = 0.5 * err_curr / ninput;

/** save errors in file to draw the
    system error with plot10 */
if (fplot10)
    fprintf(fp3, "%ld, %2.9f\n", cnt, err_curr);
    cnt++;

/* check condition for terminating learning */
result = introspective(from_snum, to_snum);
} while (result == CONTNE); /* end of long do-while */

/* update output with changed weights */

```

```

for (i=from_snum; i < to_snum; i++) forward(i);

/* for (i=0; i < nhlayer + 1; i++) {
    index = 0;
    for (j=0; j < nunit[i+1]; j++)
    {
        printf("\n\nWeights between unit %d of layer %d",
               j, j+1);
        printf(" and units of layer %d\n", i);
        for (k=0; k < nunit[i]; k++)
            printf(" %f", *(wtptr[i] + index++));
        printf("\n Threshold of unit %d of layer %d is %f",
               j, i+1, *(wtptr[i] + index++));
    }
} */

/* for (i=0; i < ninput; i++)
    for (j=0; j < noutattr; j++)
        printf("\n\n sample %d output %d = %f target %d = %f",
               i, j, outpt[i][j], target[i][j]); */
printf("\n\nTotal number of iterations is %d", cnt);
printf("\nNormalized system error is %f\n\n", err_curr);
return(result);
}

/* read in the input data file specified
   by user during interactive session */

void user_session()
{
    int i,j,showdata;
    char fnam[20], dtype[20];
    FILE *fp;

    printf("\n Start of learning session");

    /* for task with name task_name, input
       data file of the task is automatically
       set to be task_name.dat by program */
    printf("\n Enter the task name : ");
    scanf("%s", task_name);

    printf("\n How many features in input pattern? ");
    scanf("%d", &ninattr);

```

```

printf("\n How many output units?: ");
scanf("%d", &noutattr);

printf("\n Total number of input samples?: ");
scanf("%d", &ninput);

strcpy(fnam, task_name);
strcat(fnam, ".dat");

printf("\n Input file name is %s \n", fnam);
if ((fp = fopen(fnam, "r")) == NULL)
{
    printf("\nFile %s does not exist", fnam);
    exit(0);
}

printf("\n Do you want to look at data just read? (Y/N): ");
scanf("%s", dtype);
showdata = ((dtype[0] == 'y') || (dtype[0] == 'Y'));
for (i=0; i < ninput; i++) {
    for (j=0; j < ninattr; j++) {
        fscanf(fp, "%f", &input[i][j]);
        if (showdata) printf("%f ", input[i][j]);
    }
    for (j=0; j < noutattr; j++) {
        fscanf(fp, "%f", &target[i][j]);
        if (showdata) printf("%f\n", target[i][j]);
    }
}
if ((i = fclose(fp)) != 0)
{
    printf("\nFile %s cannot be closed; error %d ", fnam, i);
    exit(0);
}
}

/* main body of learning */

void learning()
{
    int result;

    user_session();
    set_up();
    init();

```

```

do {
    initwt();
    result = rumelhart(0,input);
} while (result == RESTRT);

if (result == FEXIT)
{
    printf("\n Max number of iterations reached, but failed");
    printf("\n to decrease system error sufficiently...\n");
}
dwrite(task_name);
wtwrite(task_name);
}

/* main body of output generation */
void output_generation()
{
    int i,m,nsample;
    char ans[10];
    char dfile[20];
    foutt = fopen("tqnur.mat","w");
    /* If task is already in the memory, data files
       for task do not need to be read in. But, if it
       is a new task, data files should be read in to
       reconstruct the net. */
    printf("\nGeneration of outputs for a new pattern");
    printf("\n\t Present task name is %s", task_name);
    printf("\n\t Work on a different task? (Y or N): ");
    scanf("%s", ans);
    if ((ans[0] == 'y') || (ans[0] == 'Y'))
    {
        printf("\n\t Please enter the task name: ");
        scanf("%s", task_name);
        dread(task_name);
        init();
        wtread(task_name);
    }

    /* input data for output generation
       are created */
    printf("\nEnter file name for patterns to be processed: ");
    scanf("%s", dfile);
    if ((fp1=fopen(dfile, "r")) == NULL )
    {

```



```

        perror(" Cannot open dfile ");
        exit(0);
    }

    printf("\nEnter number of patterns for processing: ");
    scanf("%d", &nsample);

    for (i=0; i < nsample; i++)
        for (m=0; m < ninattr; m++)
            fscanf(fp1, "%f", &input[i][m]);

        /* output generation calculation starts */
    for (i=0; i < nsample; i++)
    {
        forward(i);
        for (m=0; m < noutattr; m++)
            fprintf(foutt, "\n %f",
                *(outptr[nhlayer + 1] + m));
        fprintf(foutt, "");
    }
    printf("\nOutputs have been generated ");

    if ((i=fclose(fp1)) != 0)
        printf("\nFile %s cannot be closed; error %d", dfile, i);
}

/***** MAIN *****/
void main()
{
    char select[20], cont[10];

    strcpy(task_name, "*****");
    do {
        printf("\n**Select L(earning) or O(utput generation)**\n");
        do {
            scanf ("%s", select);
            switch (select[0]) {
                case 'o':
                case 'O': output_generation();
                        break;
                case 'l':
                case 'L': learning();
                        break;
                default : printf("\n Please answer");
            }
        }
    }

```

```

        printf(" learning or output generation ");
        break;
    }
} while ((select[0] != 'o') && (select[0] != 'O')
        && (select[0] != 'l') && (select[0] != 'L'));
printf("\nDo you want to continue? ");
scanf( "%s", cont);
} while ((cont[0] == 'y') || (cont[0] == 'Y'));

printf("\n\nIt is all finished. ");
printf("\nGood bye...\n\n\n ");
}

```

A.3 NINE-POINT PATH PROBLEM

```

C   A PROGRAM FOR SOLVING FOUR BAR MECHANISM
    DIMENSION TL1(10),TL2(10),TL3(10),TL4(10)
    DIMENSION TTH(10),TAL(10)
    OPEN(1, FILE = 'FBOU.T.MAT', STATUS = 'OLD')
    OPEN(2, FILE = 'FBINP.MAT', STATUS = 'NEW')
    OPEN(3, FILE = 'GTT.DAT', STATUS = 'NEW')
    TL0 = 106.0
    DO 10 I = 1,10
    READ(1,*)TL1(I),TL2(I),TL3(I),TL4(I),TTH(I),TAL(I)
10  CONTINUE
    DO 20 I = 1,10
    DO 30 J = 1,9
    PRT = TTH(I) + 40.0*(FLOAT(J)-1.0)
    DB1 = TL0*COSD(180.0) + TL1(I)*COSD(PRT)
    DB2 = TL0*SIND(180.0) + TL1(I)*SIND(PRT)
    QL4 = SQRT(DB1**2 + DB2**2)
    OL4 = ATAN2D(DB2,DB1)
    T21 = OL4 + ACOSD(((QL4**2 + TL2(I)**2 - TL3(I)**2)/
%   (2.0*QL4*TL2(I)))
    T22 = OL4 - ACOSD(((QL4**2 + TL2(I)**2 - TL3(I)**2)/
%   (2.0*QL4*TL2(I)))
    T31 = OL4 + ACOSD(((QL4**2 - TL2(I)**2 + TL3(I)**2)/
%   (2.0*QL4*TL2(I)))
    T32 = OL4 - ACOSD(((QL4**2 - TL2(I)**2 + TL3(I)**2)/
%   (2.0*QL4*TL2(I)))
    T2 = T21 - 180.0
    PX = TL1(I)*COSD(PRT) + TL4(I)*COSD(T2 + TAL(I))
    PY = TL1(I)*SIND(PRT) + TL4(I)*SIND(T2 + TAL(I))

```

```

WRITE(2,*)PX/100.
WRITE(3,*)PX/100.
WRITE(3,*)PY/100.
WRITE(2,*)PY/100.
30 CONTINUE
WRITE(3,*)TL1(I)/100.0
WRITE(3,*)TL2(I)/1000.0
WRITE(3,*)TL3(I)/1000.0
WRITE(3,*)TL4(I)/100.0
WRITE(3,*)TTH(I)/100.0
WRITE(3,*)TAL(I)/100.0
20 CONTINUE
STOP
END

```

A.4 DESIGN OF FOUR-BAR FUNCTION GENERATOR

```

C GENERATION OF y VALUES
C *****
C GIVEN LINK LENGTHS, AND CHOOSING x ARBITRARILY
C CALCULATE THETA AND THEN SOLVE A FOUR BAR MECHANISM
C CALCULATE PHI AND THEN SOLVING FOR y
C *****
C DIMENSION X(8),TH(8),PHI(8),Y(8)
C READ(1,*)RL1,RL3,(TH(I),I=1,8)
C *****
C SOLVE FOUR-BAR MECHANISM FOR PHI VALUES
C *****
C DO 20 I = 1,8
C   BX = RL0*COSD(180.0) + RL1*COSD(180 - TH(I))
C   BY = RL0*SIND(180.0) + RL1*SIND(180 - TH(I))
C   BPS = SQRT(BX*BX + BY*BY)
C   ABPS = ATAN2D(BY,BX) - 180.0
C   YJD = ACOSD((BPS**2 + RL3**2 - RL2**2)/(2.0*BPS*RL3))
C   PHI(I) = -(ABPS + YJD)
20 CONTINUE
C DO 25 I = 1,8
C   Y(I) = (PHI(I) - PHI0)*(RANY/RANPHI) + Y0
25 CONTINUE
C WRITE(3,*)(Y(I),I=1,8)
1 CONTINUE

```

```
STOP
END
```

```

PROGRAM ANSCHK
DIMENSION RT3(11)
DIMENSION X(8),TH(8),PTI(8),Y(8)
OPEN(21, FILE = 'LETax.DAT', STATUS = 'OLD')
OPEN(22, FILE = 'RT33.DAT', STATUS = 'OLD')
OPEN(23, FILE = 'WANT.MAT', STATUS = 'NEW')
READ(21,*)RANX,RANY
READ(21,*)RANTH,RANPHI
READ(21,*)TH0,PHI0,THF,PHF
READ(21,*)X0,Y0
READ(21,*)RL0
DO 11 I = 1,11
  READ(22,*)RT3(I)
11  CONTINUE
  RL1 = RT3(1)
  RL2 = RT3(2)
  RL3 = RT3(3)
  DO 467 I = 1,8
    TH(I) = RT3(I+3)
467  CONTINUE
    DO 468 I = 1,8
      X(I) = (TH(I) - TH0)*(RANX/RANTH) + X0
      WRITE(23,*)X(I)
468  CONTINUE
C *****
C SOLVE FOUR-BAR MECHANISM FOR PHI VALUES
C *****
    DO 469 I = 1,8
      BX = RL0*COSD(180.0) + RL1*COSD(180 - TH(I))
      BY = RL0*SIND(180.0) + RL1*SIND(180 - TH(I))
      BPS = SQRT(BX*BX + BY*BY)
      ABPS = ATAN2D(BY,BX) - 180.0
      YJD = ACOSD((BPS**2 + RL3**2 - RL2**2)/(2.0*BPS*RL3))
      PTI(I) = -(ABPS + YJD)
469  CONTINUE
      DO 474 I = 1,8
        Y(I) = (PTI(I) - PHI0)*(RANY/RANPHI) + Y0
        WRITE(23,*)Y(I)
474  CONTINUE
STOP

```

END

A.5 TRAJECTORY CONTROL OF A TWO-LINK MANIPULATOR

```
C *****
C POSITION CONTROL OF A TWO-LINK MANIPULATOR
C *****
C NOTE : ALL ANGLES IN RADIANs
C ALL LENGTHS IN M
C *****
C DIMENSION S(50),UVEL(50)
C DIMENSION TR1(4,4),TR2(4,4),TR3(4,4),PV(4),TR4(4,4)
C DIMENSION TR5(4,4),XY(4)
C COMMON /LINKD/ RL1,RL2,ST
C COMMON /XYC/ X(50),Y(50),I
C COMMON /XCC/ XC,YC,V_T
C COMMON /VELP/ VX(50),VY(50)
C COMMON /RMASS/ RM1,RM2
C COMMON /CONP1/ THCP1,THCP2,THDCP1,THDCP2
C COMMON /CONP2/ RKD(4),DELT
C COMMON /RMINP/
C TH_DE1(50),TH_DE2(50),THD_DE1(50),THD_DE2(50)
C COMMON /RMINQ/ TXX(2,1),TH_CP1(50),TH_CP2(50),THD_CP1(50)
C COMMON /RMINR/ THD_CP2(50)
C COMMON /VAND/ VVEL(50)
C COMMON /XCNN/ XCN(50),YCN(50)
C COMMON /VXNN/ VXN(50),VYN(50)
C COMMON /PKK/ PK1(50),PK2(50),PK3(50),PK4(50)
C OPEN(1, FILE = 'VELP.DAT', STATUS = 'OLD')
C OPEN(2, FILE = 'XY.MAT', STATUS = 'UNKNOWN')
C OPEN(9, FILE = 'CONT.PAR', STATUS = 'OLD')
C OPEN(20,FILE = 'VD.MAT', STATUS = 'UNKNOWN')
C OPEN(17,FILE = 'TH_D.MAT', STATUS = 'UNKNOWN')
C OPEN(18,FILE = 'THD_D.MAT', STATUS = 'UNKNOWN')
C OPEN(19,FILE = 'THDD_D.MAT', STATUS = 'UNKNOWN')
C OPEN(22,FILE = 'XCYC.MAT', STATUS = 'UNKNOWN')
C OPEN(45,FILE = 'VCWC.MAT', STATUS = 'UNKNOWN')
C OPEN(23,FILE = 'NORM.MAT', STATUS = 'UNKNOWN')
C OPEN(10,FILE = 'ERROR.MAT',STATUS = 'UNKNOWN')
C OPEN(16,FILE = 'GAIN.MAT',STATUS = 'UNKNOWN')
C *****
```

```

DO 1 I = 1,50
WRITE(*,*)
I CONTINUE
WRITE(*,*) 'POSITION CONTROL OF TWO LINK MANIPULATOR'
WRITE(*,*)
C LINK LENGTHS
READ(1,*)RL1,RL2
C MASS
READ(1,*)RM1,RM2
READ(1,*)ST
C RADIUS
READ(1,*)RAD
C NO OF POINTS
READ(1,*)TIME
READ(1,*)NTIME
C REQUIRED TANGENTIAL VELOCITY AND ACCELERATION FOR THE
C PROFILE
READ(1,*)V_T,ACC
C COORDINATES OF THE CENTER OF THE CIRCLE
READ(1,*)XC,YC
C INITIAL POSITION
READ(9,*)THCP1,THCP2
C INITIAL JOINT VELOCITY
READ(9,*)THDCP1,THDCP2
C INITIAL GAIN VALUES
READ(9,*)RKD(1),RKD(2),RKD(3),RKD(4)
C TIME STEP
READ(9,*)DELT
CALL TRANS(0.785398,0.0,0.0,0.0,TR1)
CALL TRANS(0.0,RL1,0.0,0.0,TR2)
CALL RMATMAT(TR1,TR2,TR3,4,4,4)
PHI = ST
STIME = 0.01
C GENERATING THE REQUIRED VELOCITY PROFILE AND
C EVALUATING THE DISTANCE TRAVELLED
DO 10 I = 1,28
IF(I.LE.9) THEN
TIME = STIME*I
C ACCELERATION PROFILE
S(I) = 0.50*ACC*(TIME)**2
WRITE(51,*)S(I)
VVEL(I) = SQRT(2.0*ACC*S(I))
V_T = VVEL(I)
ELSE IF((I.GT.9).AND.(I.LT.20)) THEN

```

```

C      CONSTANT TANGENTIAL VELOCITY PROFILE
      RLP = S(9)
      TIME = STIME*(I-9)
      VVEL(I) = 0.15
      V_T = 0.15
      S(I) = RLP + V_T*TIME
      WRITE(51,*)S(I)
      ELSE
C      DECELERATION PROFILE
      RLP = S(19)
      TIME = STIME*(I-19)
      SSG = 0.150*TIME - 0.50*(ACC)*(TIME)**2
      S(I) = RLP + SSG
      WRITE(51,*)S(I)
      VVEL(I) = SQRT(0.150**2 - 2.0*ACC*SSG)
      V_i = VVEL(I)
      END IF
      STANG = S(I)/RAD
C      WRITE(20,*)STANG
      PHI = ST + STANG
C      EVALUATING COORDINATES OF THE TRAJECTORY IN GLOBAL
C      FRAME
      CALL TRANS(PHI,0.1,0.0,0.0,TR4)
      CALL RMATMAT(TR3,TR4,TR5,i,4,4)
      PV(1) = RAD
      PV(2) = 0.00
      PV(3) = 0.00
      PV(4) = 1.00
      CALL RMATVEC(TR5,PV,XY,4,4)
      X(I) = XY(1)
      Y(I) = XY(2)
      WRITE(2,*)X(I),Y(I)
      CALL THETA_FIND
      CALL CART_VEL
      CALL THDT_FIND
10     CONTINUE
      DO 20 I = 1,27
      CALL TRAJ_CONT
20     CONTINUE
      DO 24 I = 1,27
      WRITE(10,*)TH_CP1(I)
      WRITE(10,*)TH_CP2(I)
      WRITE(10,*)THD_CP1(I)
      WRITE(10,*)THD_CP2(I)

```

```

WRITE(10,*)TH_DE1(I+1) - TH_CP1(I)
WRITE(10,*)TH_DE2(I+1) - TH_CP2(I)
WRITE(10,*)THD_DE1(I+1) - THD_CP1(I)
WRITE(10,*)THD_DE2(I+1) - THD_CP2(I)
WRITE(17,*)TH_CP1(I),TH_CP2(I)
WRITE(18,*)THD_CP1(I),THD_CP2(I)
WRITE(22,*)XCN(I+1),YCN(I+1)
WRITE(23,*)SQRT((X(I+1) - XCN(I+1))**2+(Y(I+1) -
%   YCN(I+1))**2)
WRITE(45,*)VXN(I),VYN(I)
WRITE(20,*)SQRT(VXN(I)**2+VYN(I)**2)
c   WRITE(19,*)THDD_CP1(I),THDD_CP2(I)
WRITE(16,*)PK1(I)
WRITE(16,*)PK2(I)
WRITE(16,*)PK3(I)
WRITE(16,*)PK4(I)
24  CONTINUE
STOP
END

SUBROUTINE RMATMAT(A,B,C,M,N,L)
DIMENSION A(M,L),B(L,N),C(M,N)
DO 1300 I = 1,M
DO 1300 J = 1,N
C(I,J) = 0.00
DO 1300 K = 1,L
1300 C(I,J) = C(I,J) + A(I,K)*B(K,J)
CONTINUE
RETURN
END

SUBROUTINE THETA_FIND
C   *****
C   STEP 2: FIND THE JOINT COORDINATES OF THE CIRCULAR
C   TRAJECTORY
C   *****
DIMENSION THET(4)
COMMON /LINKD/ RL1,RL2,ST
COMMON /XYC/ X(50),Y(50),I
COMMON /RMINP/
% TH_DE1(50),TH_DE2(50),THD_DE1(50),THD_DE2(50)
C   OPEN(3, FILE = 'THET.MAT', STATUS = 'UNKNOWN')
*****
RJJ = 2.0 * Y(I) * RL1

```



```

RII = 2.0 * X(I) * RL!
RKK = X(I)*X(I) + Y(I)*Y(I) + RL1*RL1 - RL2*RL2
RTT = RJJ*RJJ + RII*RII - RKK*RKK
THET(1) = ATAN2(RJJ,RII) + ATAN2(SQRT(RTT),RKK)
PAR1 = Y(I) - RL1*SIN(THET(1))
PAR2 = X(I) - RL1*COS(THET(1))
THET(2) = ATAN2(PAR1,PAR2) - THET(1)
WRITE(3,*)THET(1),THET(2)
TH_DE1(I) = THET(1)
TH_DE2(I) = THET(2)
RETURN
END

```

SUBROUTINE CART_VEL

```

C *****
C STEP 3: RESOLVE TANGENTIAL VELOCITY V_T IN THE
c GLOBAL COORDINATE SYSTEM
C *****
DIMENSION VP(3)
COMMON /LINKD/ RL1,RL2,ST
COMMON /XYC/ X(50),Y(50),I
COMMON /XCC/ XC,YC,V_T
COMMON /VELP/ VX(50),VY(50)
OPEN(4, FILE = 'VEL.MAT', STATUS = 'UNKNOWN')
OPEN(7, FILE = 'PNV.MAT', STATUS = 'UNKNOWN')
PKL = Y(I)-YC
PKK = X(I)-XC
ALPH = ATAN2(PKL,PKK)
VP(1) = V_T*COS(1.570796327+ALPH)
VP(2) = V_T*COS(ALPH)
VP(3) = 1.0
WRITE(4,*)VP(1),VP(2)
VX(I) = VP(1)
VY(I) = VP(2)
PNORMV = SQRT(VX(I)**2+VY(I)**2)
WRITE(7,*)PNORMV
RETURN
END

```

SUBROUTINE THDT_FIND

```

C *****
C STEP 4: EVALUATE THE ROTATION RATES THDT_K1 AND THDT_K2
C USING JACOBIAN MATRIX

```

```

C *****
  DIMENSION VPG(2),THDT(2),RINV(2,2)
  COMMON /LINKD/ RL1,RL2,ST
  COMMON /XYC/ X(50),Y(50),I
  COMMON /RMINP/
% TH_DE1(50),TH_DE2(50),THD_DE1(50),THD_DE2(50)
  COMMON /XCC/ XC,YC,V_T
  COMMON /VELP/ VX(50),VY(50)
  OPEN(8, FILE = 'THDT.MAT', STATUS = 'UNKNOWN')
  VPG(1) = VX(I)
  VPG(2) = VY(I)
  UT11 = -RL1*SIN(TH_DE1(I)) - RL2*SIN(TH_DE1(I)+TH_DE2(I))
  UT12 = -RL2*SIN(TH_DE1(I)+TH_DE2(I))
  UT21 = RL1*COS(TH_DE1(I)) + RL2*COS(TH_DE1(I)+TH_DE2(I))
  UT22 = RL2*COS(TH_DE1(I)+TH_DE2(I))
  DET = UT11*UT22 - UT21*UT12
  RINV(1,1) = UT22/DET
  RINV(1,2) = -UT12/DET
  RINV(2,1) = -UT21/DET
  RINV(2,2) = UT11/DET
  CALL RMATVEC(RINV,VPG,THDT,2,2)
  WRITE(8,*)THDT(1),THDT(2)
  THD_DE1(I) = THDT(1)
  THD_DE2(I) = THDT(2)
  RETURN
END

SUBROUTINE TRAJ_CONT
C *****
C STEP 5: TRAJECTORY CONTROL OF TWO-LINK MANIPULATOR
C *****
  DIMENSION RX(4),XSTRT(4),RMAX(4),RMIN(4),RPHI(4)
  DIMENSION RPSI(1),RW(44),XCP(50),YCP(50)
  COMMON /LINKD/ RL1,RL2,ST
  COMMON /XYC/ X(50),Y(50),I
  COMMON /XCC/ XC,YC,V_T
  COMMON /VELP/ VX(50),VY(50)
  COMMON /RMINP/
% TH_DE1(50),TH_DE2(50),THD_DE1(50),THD_DE2(50)
  COMMON /RMINQ/ TXX(2,1),TH_CP1(50),TH_CP2(50),THD_CP1(50)
  COMMON /RMINR/ THD_CP2(50)
  COMMON /SEEK/ IDATA,IPRINT,NSHOT,NTEST,MAXM,F,G,TOL,
% ZERO,R,REDUCE
  COMMON /CONP1/ THCP1,THCP2,THDCP1,THDCP2

```

```

COMMON /CONP2/ RKD(4),DELT
COMMON /PKK/ PK1(50),PK2(50),PK3(50),PK4(50)
IDATA = 0
IPRINT = 0
TH_CP1(1) = THCP1
TH_CP2(1) = THCP2
THD_CP1(1) = THDCP1
THD_CP2(1) = THDCP2
C *****
C FIND THE OPTIMUM VALUE OF RKD THAT GIVES MINIMUM
C ERROR IN POSITION
C *****
C *****
C CALLING SIDDALL LIBRARY ROUTINE
C *****
JN = 4
JNCONS = 0
JNEQUS = 0
JNPENAL = 5
F = 0.001
G = 0.001
MAXM = 25000
DATA RMAX/1.0e3,1.0e3,1.0e3,1.0e3/
DATA RMIN/-1.0e3,-1.0e3,-1.0e3,-1.0e3/
DO 775 KK = 1,4
XSTRT(KK) = RKD(KK)
775 CONTINUE
PRINT *, 'ITER = ', I
CALL SEEK(JN,JNCONS,JNEQUS,JNPENAL,RMAX,RMIN,XSTRT,RX,
% RU,RPHI,RPSI,JNVIOL,RW)
PK1(I) = RX(1)
PK2(I) = RX(2)
PK3(I) = RX(3)
PK4(I) = RX(4)
RETURN
END

SUBROUTINE UREAL(RX,RU)
DIMENSION RX(1)
DIMENSION QM(2,2),QV(2,2),QG(2,2),QT1(2,1),QT2(2,1)
DIMENSION THDDT1(2,1),QMI(2,2),THDD_CP1(50)
DIMENSION THDD_CP2(50),TORI(2)
DIMENSION XU(2,2),TDZ(2),VPN(2)
COMMON /LINKD/ RL1,RL2,ST

```

```

COMMON /RMINP/
%      TH_DE1(50),TH_DE2(50),THD_DE1(50),THD_DE2(50)
COMMON /RMINQ/ TXX(2,1),TH_CP1(50),TH_CP2(50),THD_CP1(50)
COMMON /RMINR/ THD_CP2(50)
COMMON /XYC/ X(50),Y(50),I
COMMON /RMAS/ RM1,RM2
COMMON /CONP2/ RKD(4),DELT
COMMON /XCC/ XC,YC,V_T
COMMON /VELP/ VX(50),VY(50)
COMMON /XCNN/ XCN(50),YCN(50)
COMMON /VXNN/ VXN(50),VYN(50)
C      *****
C      GH = 9.81
C      *****
C      CALCULATING TORQUE BASED ON ERROR IN POSITION
C      *****
%      XCN(1) = RL1*COS(TH_CP1(1)) + RL2*COS(TH_CP1(1) +
%          TH_CP2(1))
%      YCN(1) = RL1*SIN(TH_CP1(1)) + RL2*SIN(TH_CP1(1) +
%          TH_CP2(1))

      IF(I.EQ.2) THEN
      END IF
      TORI(1) = RX(1)*(TH_DE1(I+1) - TH_CP1(I)) +
%      RX(3)*(THD_DE1(I+1) - THD_CP1(I))
      TORI(2) = RX(2)*(TH_DE2(I+1) - TH_CP2(I)) +
%      RX(4)*(THD_DE2(I+1) - THD_CP2(I))
C      *****
C      CALCULATE THDDT AT TIME T
C      *****
      CALL STHEK(TH_CP1,TH_CP2,THD_CP1,THD_CP2,
%      THDDTI,I,TORI)
      THDD_CP1(I) = THDDTI(1,1)
      THDD_CP2(I) = THDDTI(2,1)
C      *****
C      HERE WE KNOW THET, THDT AND THDDT AT TIME T
C      *****
C      CALCULATE THEDDT AT TIME T+DELT
C      *****
C      CALCULATE THET,THDT AT TIME T+DELT
C      *****
      TORI(1) = RX(1)*(TH_DE1(I+1) - TH_DE1(I)) +
%      RX(3)*(THD_DE1(I+1) - THD_DE1(I))
      TORI(2) = RX(2)*(TH_DE2(I+1) - TH_DE2(I)) +

```

```

%          RX(4)*(THD_DE2(I+1) - THD_DE2(I))
CALL STHEK(TH_CP1,TH_CP2,THD_CP1,THD_CP2,
%      THDDTI,I+1,TORI)
THDD_CP1(I+1) = THDDTI(1,I)
THDD_CP2(I+1) := THDDTI(2,I)
C *****
ALP = 0.5
BET = 0.001
THD_CP1(I+1) = THD_CP1(I) + (1.0-BET)*THDD_CP1(I)*DELTA +
%      BET*THDD_CP1(I+1)*DELTA
THD_CP2(I+1) = THD_CP2(I) + (1.0-BET)*THDD_CP2(I)*DELTA +
%      BET*THDD_CP2(I+1)*DELTA
TH_CP1(I+1) = TH_CP1(I) + THD_CP1(I)*DELTA +
%      ((0.5-ALP)*THDD_CP1(I) + ALP*THDD_CP1(I+1))*DELTA**2
TH_CP2(I+1) = TH_CP2(I) + THD_CP2(I)*DELTA +
%      ((0.5-ALP)*THDD_CP2(I) + ALP*THDD_CP2(I+1))*DELTA**2
C *****
XCN(I+1) = RL1*COS(TH_CP1(I+1)) + RL2*COS(TH_CP1(I+1) +
%      TH_CP2(I+1))
YCN(I+1) = RL1*SIN(TH_CP1(I+1)) + RL2*SIN(TH_CP1(I+1) +
%      TH_CP2(I+1))
TDZ(1) = THD_CP1(I+1)
TDZ(2) = THD_CP2(I+1)
XU(1,1) = -RL1*SIN(TH_CP1(I+1)) - RL2*SIN(TH_CP1(I+1)
%      + TH_CP2(I+1))
XU(1,2) = -RL2*SIN(TH_CP1(I+1)+TH_CP2(I+1))
XU(2,1) = RL1*COS(TH_CP1(I+1)) - RL2*COS(TH_CP1(I+1)
%      + TH_CP2(I+1))
XU(2,2) = RL2*COS(TH_CP1(I+1)+TH_CP2(I+1))
CALL RMATVEC(XU,TDZ,VPN,2,2)
VXN(I+1) = VPN(1)
VYN(I+1) = VPN(2)
QW1 = ((X(I+1) - XCN(I+1))*10.0)**2
QW2 = ((Y(I+1) - YCN(I+1))*10.0)**2
QW3 = ((VX(I+1) - VXN(I+1)))**2
QW4 = ((VY(I+1) - VYN(I+1)))**2
RU = ((QW1 + QW2)*1.0 + QW3 + QW4)*1.0e6
RETURN
END

SUBROUTINE STHEK(TH_CP1,TH_CP2,THD_CP1,THD_CP2,
%      THDDTI,I,TORI)
DIMENSION QM(2,2),QV(2,2),QG(2,2),QT1(2,1),QT2(2,1)

```

```

      DIMENSION THDDTI(2,1),QMI(2,2)
      DIMENSION TH_CP1(50),THD_CP1(50)
      DIMENSION TH_CP2(50),THD_CP2(50)
      DIMENSION XU(2,2),TDZ(2),VPN(2)
      DIMENSION RX(4),TORJ(2)
      COMMON /LINKD/ RL1,RL2,ST
      COMMON /RMASS/ RM1,RM2
C *****
      GH = 9.81
      QM(1,1) = RL2**2*RM2 + 2.0*RL1*RL2*RM2*COS(TH_CP2(I))
%   + RL1**2*(RM1 + RM2)
      QM(1,2) = RL2**2*RM2 + RL1*RL2*RM2*COS(TH_CP2(I))
      QM(2,1) = RL2**2*RM2 + RL1*RL2*RM2*COS(TH_CP2(I))
      QM(2,2) = RL2**2*RM2
      QV(1,1) = -RM2*RL1*RL2*SIN(TH_CP2(I))*THD_CP2(I)**2 -
%   2.0*RM2*RL1*RL2*SIN(TH_CP2(I))*THD_CP1(I)*THD_CP2(I)
      QV(2,1) = RM2*RL1*RL2*SIN(TH_CP2(I))*THD_CP1(I)**2
      QG(1,1) = RM2*RL2*GH*COS(TH_CP1(I)+TH_CP2(I)) +
%   (RM1 + RM2)*RL1*GH*COS(TH_CP1(I))
      QG(2,1) = RM2*RL2*GH*COS(TH_CP1(I) + TH_CP2(I))
      CALL QMINV(QM,QMI)
      CALL RMATADD(QV,QG,QT1,2,1)
      CALL RMATSUB(TORI,QT1,QT2,2,1)
      CALL RMATVEC(QMI,QT2,THDDTI,2,2)
      RETURN
      END

      SUBROUTINE CONST(RX,JNCONS,RPHI)
      DIMENSION RX(1),RPHI(1)
      RETURN
      END

      SUBROUTINE EQUAL(RX,RPSI,JNEQUS)
      DIMENSION RX(1),RPSI(1)
      RETURN
      END

      SUBROUTINE QMINV(QM,QMI)
      DIMENSION QM(2,2),QMI(2,2)
      DO 410 I = 1,2
      DO 410 J = 1,2
      QMI(I,J) = 0.0

```

```

410  CONTINUE
      QMP = QM(1,1)*QM(2,2) - QM(1,2)*QM(2,1)
      QMI(1,1) = QM(2,2)/QMP
      QMI(1,2) = -QM(1,2)/QMP
      QMI(2,1) = -QM(2,1)/QMP
      QMI(2,2) = QM(1,1)/QMP
      RETURN
      END

C *****
C  TO NORMALIZE THE INPUT AND OUTPUT VECTOR
C *****
      DIMENSION PIN1(50),PIN2(50),PIN3(50),PIN4(50)
      DIMENSION PIN5(50),PIN6(50),PIN7(50),PIN8(50)
      DIMENSION PON1(50),PON2(50),PON3(50),PON4(50)
      OPEN(UNIT=1,FILE='ERROR.MAT',STATUS='OLD')
      OPEN(UNIT=2,FILE='GAIN.MAT',STATUS='OLD')
      OPEN(UNIT=3,FILE='INP.DAT',STATUS='UNKNOWN')
      OPEN(UNIT=4,FILE='OUT.DAT',STATUS='UNKNOWN')
      DO 10 I = 1,27
        READ(1,*)PIN1(I),PIN2(I),PIN3(I),PIN4(I)
        READ(1,*)PIN5(I),PIN6(I),PIN7(I),PIN8(I)
        READ(2,*)PON1(I),PON2(I),PON3(I),PON4(I)
10    CONTINUE
      CALL MINMAX(PIN1,SMALL1,PLARGE1,27)
      PRINT *,SMALL1,PLARGE1
      CALL MINMAX(PIN2,SMALL2,PLARGE2,27)
      PRINT *,SMALL2,PLARGE2
      CALL MINMAX(PIN3,SMALL3,PLARGE3,27)
      PRINT *,SMALL3,PLARGE3
      CALL MINMAX(PIN4,SMALL4,PLARGE4,27)
      PRINT *,SMALL4,PLARGE4
      CALL MINMAX(PIN5,SMALL5,PLARGE5,27)
      PRINT *,SMALL5,PLARGE5
      CALL MINMAX(PIN6,SMALL6,PLARGE6,27)
      PRINT *,SMALL6,PLARGE6
      CALL MINMAX(PIN7,SMALL7,PLARGE7,27)
      PRINT *,SMALL7,PLARGE7
      CALL MINMAX(PIN8,SMALL8,PLARGE8,27)
      PRINT *,SMALL8,PLARGE8
      CALL MINMAX(PON1,SMALL9,PLARGE9,27)
      PRINT *,SMALL9,PLARGE9

```

```

CALL MINMAX(PON2,SMALL10,PLARGE10,27)
PRINT *,SMALL10,PLARGE10
CALL MINMAX(PON3,SMALL11,PLARGE11,27)
PRINT *,SMALL11,PLARGE11
CALL MINMAX(PON4,SMALL12,PLARGE12,27)
PRINT *,SMALL12,PLARGE12
DO 20 I = 1,27
SDOT1 = (PIN1(I) - SMALL1)/(PLARGE1 - SMALL1)
SDOT2 = (PIN2(I) - SMALL2)/(PLARGE2 - SMALL2)
SDOT3 = (PIN3(I) - SMALL3)/(PLARGE3 - SMALL3)
SDOT4 = (PIN4(I) - SMALL4)/(PLARGE4 - SMALL4)
SDOT5 = (PIN5(I) - SMALL5)/(PLARGE5 - SMALL5)
SDOT6 = (PIN6(I) - SMALL6)/(PLARGE6 - SMALL6)
SDOT7 = (PIN7(I) - SMALL7)/(PLARGE7 - SMALL7)
SDOT8 = (PIN8(I) - SMALL8)/(PLARGE8 - SMALL8)
SDOT9 = (PON1(I) - SMALL9)/(PLARGE9 - SMALL9)
SDOT10 = (PON2(I) - SMALL10)/(PLARGE10 - SMALL10)
SDOT11 = (PON3(I) - SMALL11)/(PLARGE11 - SMALL11)
SDOT12 = (PON4(I) - SMALL12)/(PLARGE12 - SMALL12)
WRITE(3,*)SDOT1
WRITE(3,*)SDOT2
WRITE(3,*)SDOT3
WRITE(3,*)SDOT4
WRITE(3,*)SDOT5
WRITE(3,*)SDOT6
WRITE(3,*)SDOT7
WRITE(3,*)SDOT8
WRITE(4,*)SDOT9
WRITE(4,*)SDOT10
WRITE(4,*)SDOT11
WRITE(4,*)SDOT12
20 CONTINUE
STOP
END

C A LP APPROACH FOR NEURAL NETWORKS
C *****
C YW = N + 4*(N + NCONS + NEQUS)
C   WHERE N = NUMBER OF DESIGN VARIABLES = 1
C   NCONS = NUMBER OF INEQUALITY CONSTRAINTS = 1
C   NEQUS = NUMBER OF EQUALITY CONSTRAINTS = 1
C YW = 1 + 4*(1+1+1) = 13
C L.P.
C ZW = M*(5+M)

```



```

C      - WHERE M IS NUMBER OF CONSTRAINING EQUATIONS = ROWS
C      WHICH IS DEFINED BELOW
C      *****
C      ZW = 36*(5+36) = 1476
C      *****
C      DIMENSIONS FOR [A] MATRIX
C      ROWS = (NO.OF OUTPUT)*TOTAL.NO.OF TRIALS
C      = 4 * (9) = 36
C      COLUMNS = (NO.OF INPUT*2 + 4)*NO.OF OUTPUT
C      = (8*2 + 4)*4 = 80
C      *****
C      DIMENSION YX(1),YXSTR(1),RMAX(1),RMIN(1),PHI(1),PSI(1)
C      DIMENSION YW(50),ZX(80),ZA(36,80),ZB(36),ZC(80)
C      DIMENSION ZAP(36,80),ZCP(80),ZBP(36),ZW(1476)
C      DIMENSION BBW(4,8),BBC(4),BBD(4),ZTOB(8)
C      COMMON
% /SEEK/IDATA,IPRINT,NSHOT,NTEST,MAXM,F,G,TOL,ZERO,
% R,REDUCE
COMMON /BL1/ZC,ZX,ZW,ZAP,ZCP,ZBP
COMMON /BL3/ZB
COMMON /BL2/MZ,NZ,NUTS,NT,NI,NOUT,NOI
COMMON /FAL/ZTOB
COMMON /ANT/ZA
OPEN(2, FILE = 'SCOUT-T.DAT', STATUS = 'OLD')
OPEN(3, FILE = 'CLPTA.OUT', STATUS = 'OLD')
OPEN(14, FILE = 'LIN.DAT', STATUS = 'OLD')
READ(14,*)MZ
READ(14,*)NZ
READ(14,*)NUTS
READ(14,*)NT,NI
READ(14,*)NOUT,NOI
MAXM = 10000
CALL ALPG
1 WRITE(*,*)
DO 196 I = 1,MZ
196 READ(2,*)ZB(I)
CONTINUE
READ(3,*)(ZC(I),I = 1,NZ)
F = 0.001
G = 0.01
NY = 1
NCONS = 0
NEQUS = 0
NPENAL = 3

```

```

IDATA = 0
DATA RMAX/0.10/
DATA RMIN/-0.10/
DATA YXSTRT/0.0013427/
NOISE = 1
CALL
% SEEK(NY,NCONS,NEQUS,NPENAL,RMAX,RMIN,YXSTRT,YX,YU,PHI,
% PSI,NVIOL,YW)
CALL ANSWER(YU,YX,PHI,PSI,NY,NCONS,NEQUS)
WRITE(*,*)'DO YOU WISH TO CONTINUE ?'
WRITE(*,*)'1: YES '
WRITE(*,*)'2: NO '
READ(*,*)NDEC
IF(NDEC.EQ.1) THEN
GO TO 1
ELSE
END IF
STOP
END

SUBROUTINE UREAL(YX,YU)
DIMENSION YX(1),YXSTRT(1),RMAX(1),RMIN(1),PHI(1),PSI(1)
DIMENSION YW(50),ZX(80),ZA(36,80),ZB(36),ZC(80)
DIMENSION ZAP(36,80),ZBP(36),ZCP(80)
DIMENSION ZW(1476),ZTOB(8)
DIMENSION BBW(4,8),BBC(4),BBD(4),D(2)
DIMENSION SAK(4),RT3(4),ZZTOB(4)
COMMON /BL1/ZC,ZX,ZW,ZAP,ZCP,ZBP
COMMON /BL3/ZB
COMMON /BL2/MZ,NZ,NUTS,NT,NI,NOUT,NOI
COMMON /SIMPLE/NSTOP,IDATA,NINDEX
COMMON /PAKS/BBW,BBC,BBD
COMMON /FAL/ZTOB
COMMON /ANT/ZA
COMMON /DEPUT/D,RMX,RMN
OPEN(15, FILE = 'SCINP-N.DAT', STATUS = 'OLD')
OPEN(9, FILE = 'SCOUT-N.DAT', STATUS = 'OLD')
OPEN(19, FILE = 'PERC.MAT', STATUS = 'NEW')
OPEN(18, FILE = 'OBJ.MAT', STATUS = 'NEW')
IDATA = 0
NSTOP = 3000
NINDEX = 1
DO 20 I = 1,MZ
KR = 1

```

```

DO 30 J = 1,NZ
IF(J.GT.(20*KR)) THEN
KR = KR + 1
END IF
IF((J.GE.(1+20*(KR-1))).AND.(J.LT.(17+20*(KR-1)))) THEN
ZAP(I,J) = YX(1)*ZA(I,J)
ELSE
ZAP(I,J) = ZA(I,J)
END IF
30 CONTINUE
20 CONTINUE
SQM = 0.0
DO 40 I = 1,MZ
ZBP(I) = YX(1)*ZB(I)
SQM = SQM + ZB(I)
40 CONTINUE
KR = 1
DO 50 J = 1,NZ
IF(J.GT.(20*KR)) THEN
KR = KR + 1
END IF
IF((J.GE.(1 + 20*(KR-1))).AND.(J.LT.(17+20*(KR-1)))) THEN
ZCP(J) = YX(1)*ZC(J)
ELSE
ZCP(J) = ZC(J)
END IF
50 CONTINUE
CALL SIMPLE(NZ,MZ,ZAP,ZBP,ZCP,ZX,ZU,ZW)
XX = 0.0
DO 501 J = 1,NZ
XX = XX + ZCP(J)*ZX(J)
501 CONTINUE
YYU = SQM - XX
WRITE(*,*)'L.P. OBJECTIVE FUNCTION IS',YYU
c CALL WASS(ZX,BBW,BBC,BBD)
YT1 = 0.0
YT2 = 0.0
YT3 = 0.0
DO 55 NM = 1,16,2
DO 60 MM = NM,8C,20
YT1 = YX(1)*(ZC(NM)*ZX(MM)) + YT1
60 CONTINUE
55 CONTINUE
DO 65 NM = 2,16,2

```

```

8      DO 70 MM = NM,80,20
      YT2 = YX(1)*(ZC(NM)*ZX(MM)) + YT2
70     CONTINUE
65     CONTINUE
      DO 75 NM = 17,20
      DO 80 MM = NM,80,20
      YT3 = (ZC(NM)*ZX(MM)) + YT3
80     CONTINUE
75     CONTINUE
      YT4 = YX(1)*SQM
C      CALL RMIXD(BBW,BBC,BBD,YX,ZTOB,RT3)
      YU = (YT1 + YT2 + YT3 - YT4)**4
      WRITE(*,*)'SLOPE IS',YX(1)
      WRITE(*,*)'SEEK OBJECTIVE FUNCTION IS',YU
      IF (NSW.EQ.1) THEN
      STOP
      END IF
      IF(YU.LT.(6.0E-6)) THEN
      DO 881 ISK = 1,9
      DO 884 I = 1,8
      READ(15,*)ZTOB(I)
884     CONTINUE
      DO 886 I = 1,4
      READ(9,*)ZZTOB(I)
886     CONTINUE
      CALL WASS(ZX,BBW,BBC,BBD)
      CALL RMIXD(BBW,BBC,BBD,YX,ZTOB,RT3)
      DO 923 JK = 1,4
      WRITE(19,*)ZZTOB(JK),RT3(JK)
      WRITE(18,*)RT3(JK)
923     CONTINUE
881     CONTINUE
      NSW = 1
      ELSE
      END IF
      RETURN
      END

      SUBROUTINE CONST(YX,NCONS,PHI)
      DIMENSION PHI(1),D(2),YX(1)
      COMMON /DEPUT/D,RMX,RMN
      NOISE = NOISE + 1
      RETURN

```

```

      EN'D

      SUBROUTINE EQUAL(YX,PSI,NEQUS)
      DIMENSION YX(1),PSI(1)
      RETURN
      END

      SUBROUTINE RMATMUL(A,B,C,M,N)
      DIMENSION A(M,N),B(N),C(M)
      DO 4430 I = 1,M
      C(I) = 0.0
      DO 4440 J = 1,N
      C(I) = C(I) + A(I,J)*B(J)
4440 CONTINUE
4430 CONTINUE
      RETURN
      END

      SUBROUTINE ALPG
      GENERATION OF [A] MATRIX FOR LINEAR PROGRAMMING
      DIMENSION X(8),ZA(36,80)
      COMMON /ANT/ZA
      OPEN(17, FILE = 'SCINP-T.DAT', STATUS = 'OLD')
      DO 1050 NI = 1,20,4
      KNI = NI
      NS = 1
      NT = 16
      DO 714 I = 1,8
      READ(17,*)X(I)
714 CONTINUE
780 CONTINUE
      IF(NT.GT.80) GOTO 7100
      MT = 1
      DO 710 I = NS,NT,2
      ZA(KNI,I) = X(MT)
      MT = MT + 1
710 CONTINUE
      MT = 1
      DO 720 I = NS+1,NT,2
      ZA(KNI,I) = -X(MT)
      MT = MT + 1
720 CONTINUE
      DO 730 I = NT+1,NT+4

```

```

      ZA(KNI,I) = 1.0
730  CONTINUE
      DO 740 I = NT+2,NT+3
      ZA(KNI,I) = -1.0
740  CONTINUE
      KNI = KNI + 1
      NS = NS + 20
      NT = NT + 20
      GO TO 780
7100 CONTINUE
1050 CONTINUE
      RETURN
      END

C *****
C   TO SCALE BACK THE GAIN AND ERROR VALUES
C   OBTAINED FROM THE NEURAL NETWORK
C *****
      DIMENSION GNR1(50),GNR2(50),GNR3(50),GNR4(50)
      DIMENSION PON1(50),PON2(50),PON3(50),PON4(50)
      OPEN(UNIT=1, FILE='GAIN.MAT', STATUS='OLD')
      OPEN(UNIT=2, FILE='SCKF-N.DAT', STATUS = 'OLD')
      OPEN(UNIT=3, FILE='KFRM-N.DAT', STATUS = 'UNKNOWN')
      DO 10 I = 1,27
      READ(1,*)PON1(I),PON2(I),PON3(I),PON4(I)
      READ(2,*)GNR1(I)
      READ(2,*)GNR2(I)
      READ(2,*)GNR3(I)
      READ(2,*)GNR4(I)
10  CONTINUE
      CALL MINMAX(PON1,SMALL9,PLARGE9,27)
      PRINT *,SMALL9,PLARGE9
      CALL MINMAX(PON2,SMALL10,PLARGE10,27)
      PRINT *,SMALL10,PLARGE10
      CALL MINMAX(PON3,SMALL11,PLARGE11,27)
      PRINT *,SMALL11,PLARGE11
      CALL MINMAX(PON4,SMALL12,PLARGE12,27)
      PRINT *,SMALL12,PLARGE12
      DO 20 I = 1,27
      GAIN1 = GNR1(I)*(PLARGE9-SMALL9) + SMALL9
      GAIN2 = GNR2(I)*(PLARGE10-SMALL10) + SMALL10
      GAIN3 = GNR3(I)*(PLARGE11-SMALL11) + SMALL11
      GAIN4 = GNR4(I)*(PLARGE12-SMALL12) + SMALL12
      WRITE(3,*)GAIN1,GAIN2,GAIN3,GAIN4

```

```

20  CONTINUE
    STOP
    END

```

```

C *****
C  MATLAB FILES TO CHECK FOR THE TRAJECTORY USING
C  THE GAIN VALUES OBTAINED FROM LP-NEURO METHOD
c  AND AS WELL AS FROM OPTIMIZATION ROUTINE
C *****
C          final.m
C *****

clear
load thet.dat
load thdt.dat
load gain.dat
load xy.dat
load xcyc.dat
l1 = 0.3;
l2 = 0.2;
m1 = 4.0;
m2 = 3.0;
g = 9.81;
for i = 1:27
    t1 = thet(i,1);
    t11 = thet(i+1,1);
    t2 = thet(i,2);
    t22 = thet(i+1,2);
    td1 = thdt(i,1);
    td11 = thdt(i+1,1);
    td2 = thdt(i,2);
    td22 = thdt(i+1,2);
    m(1,1) = l2^2*m2 + 2*l1*l2*m2*cos(t2) + l1^2*(m1 + m2);
    m(1,2) = l2^2*m2 + l1*l2*m2*cos(t2);
    m(2,1) = l2^2*m2 + l1*l2*m2*cos(t2);
    m(2,2) = l2^2*m2;
    v(1,1) = -m2*l1*l2*sin(t2)*td2^2 - 2*m2*l1*l2*sin(t2)*td1*td2;
    v(2,1) = m2*l1*l2*sin(t2)*td1^2;
    gg(1,1) = m2*l2*g*cos(t1+t2) + (m1+m2)*l1*g*cos(t1);
    gg(2,1) = m2*l2*g*cos(t1+t2);
    e1 = t11 - t1;
    e2 = td11 - td1;
    e3 = t22 - t2;
    e4 = td22 - td2;
    K1 = gain(i,1);

```

```

K2 = gain(i,2);
K3 = gain(i,3);
K4 = gain(i,4);
to(1,1) = K1*e1 + K3*e2;
to(2,1) = K2*e3 + K4*e4;
ja = inv(m)*(to - v - gg);
al = 0.5;
be = 0.001;
delt = 0.001;
fr
jv(1,1) = td1 + (1-be)*ja(1,1)*delt + be*jan(1,1)*delt ;
jv(2,1) = td2 + (1-be)*ja(2,1)*delt + be*jan(2,1)*delt;
jd(1,1) = t1 + td1*delt + ((0.5-al)*ja(1,1) + al*jan(1,1))*delt^2;
jd(2,1) = t2 + td2*delt + ((0.5-al)*ja(2,1) + al*jan(2,1))*delt^2;
thet(i+1,1) = jd(1,1);
thet(i+1,2) = jd(2,1);
%thdt(i+1,1) = jv(1,1);
%thdt(i+1,2) = jv(2,1);
x(i,1) = l1*cos(jd(1,1)) + l2*cos(jd(1,1) + jd(2,1));
y(i,1) = l1*sin(jd(1,1)) + l2*sin(jd(1,1) + jd(2,1));
jcb(1,1) = -l1*sin(jd(1,1)) - l2*sin(jd(1,1)+jd(2,1));
jcb(1,2) = -l2*sin(jd(1,1) + jd(2,1));
jcb(2,1) = l1*cos(jd(1,1)) + l2*cos(jd(1,1) +jd(2,1));
jcb(2,2) = l2*cos(jd(1,1) + jd(2,1));
vx(i,1) = jcb(1,1) * jv(1,1) + jcb(1,2)*jv(2,1);
vy(i,1) = jcb(2,1) * jv(1,1) + jcb(2,2)*jv(2,1);
vd(i,1) = sqrt(vx(i,1)^2 + vy(i,1)^2);
%ex(i,1) = xy(i+1,1) - xcyc(i,1);
%ey(i,1) = xy(i+1,2) - xcyc(i,2);
%nex(i,1) = xy(i+1,1) - x(i,1);
%ney(i,1) = xy(i+1,2) - y(i,1);
%er_op(i,1) = sqrt(ex(i,1)^2 + ey(i,1)^2);
%er_lp(i,1) = sqrt(nex(i,1)^2 + ney(i,1)^2);
end

```

```

c *****
c                                     fr.m
c *****
c
load pthet.dat
load pthdt.dat
load gain.dat
pt1 = pthet(i,1);
pt11 = pthet(i+1,1);

```



```

pt2 = pthet(i,2);
pt22 = pthet(i+1,2);
ptd1 = pthdt(i,1);
ptd11 = pthdt(i+1,1);
ptd2 = pthdt(i,2);
ptd22 = pthdt(i+1,2);
pm(1,1) = l2^2*m2 + 2*l1*l2*m2*cos(pt2) + l1^2*(m1+m2);
pm(1,2) = l2^2*m2 + l1*l2*m2*cos(pt2);
pm(2,1) = l2^2*m2 + l1*l2*m2*cos(pt2);
pm(2,2) = l2^2*m2;
pv(1,1) = -m2*l1*l2*sin(pt2)*ptd2^2 - 2*m2*l1*l2*sin(pt2)*ptd1*ptd2;
pv(2,1) = m2*l1*l2*sin(pt2)*ptd1^2;
pgg(1,1) = m2*l2*g*cos(pt1+pt2) + (m1+m2)*l1*g*cos(pt1);
pgg(2,1) = m2*l2*g*cos(pt1+pt2) ;
pe1 = pt11 - pt1;
pe2 = ptd11 - ptd1;
pe3 = pt22 - pt2;
pe4 = ptd22 - ptd2;
pK1 = gain(i,1);
pK2 = gain(i,2);
pK3 = gain(i,3);
pK4 = gain(i,4);
pto(1,1) = pK1*pe1 + pK3*pe2;
pto(2,1) = pK2*pe3 + pK4*pe4;
jan = inv(pm)*(pto - pv - pgg);

```

4

